High-Voltage Intelligent Power Devices Application Note

TPD4163K, TPD4163F TPD4164K, TPD4164F TPD4165K

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1. Applicapable products

1.1. Product overview

TPD4163K, TPD4163F, TPD4164K, TPD4164F and TPD4165K are high voltage intelligence devices and they are single chip inverter ICs using TOSHIBA original trench-isolation-type high-voltage SOI (Silicon on insulator) process.

Each product has control circuit such as IGBT gate drive circuit, bootstrap circuit for high side gate drive power supply, various protection circuits, level shift circuit and logic circuit. And it has also 6 pieces of IGBT and FRD in single chip device. It has function of direct driving of three phase brushless DC motor. It is the optimal product for motor drive in home appliance.

The HVIPDs can be used in combining with Toshiba's microcomputer or motor controller IC to drive a motor with sine-wave (180° commutation) type so as to achieve low noise and low vibration.



Figure 1.1.1 High-voltage intelligent power devices

1.2. Applicable product list

| | | | Out charac | tput teristic | | | | Functio | n | | |
|-----------------|---------|---------|---|-------------------------------------|---------|--|------------------|--------------------------------|---------------------|--------------------------------|---------------------------------|
| Product name | Rating | Package | Output saturation voltage (Typ.) | FRD forward voltage (Typ.) | 6-input | 3-Phase Distribution PWM Circuit | Current limit | over- current Protection | Thermal Shutdown | Under voltage Protection | Shutdown (SD) pin control |
| TPD4163K | 600V/1A | HDIP30 | 2.6V (Ic=0.5A) | 2.0V (IF=0.5A) | ~ | - | - | ~ | ~ | ~ | ~ |
| TPD4163F | 600V/1A | HSSOP31 | 2.6V (Ic=0.5A) | 2.0V (IF=0.5A) | ~ | _ | - | ~ | ~ | ~ | ~ |
| TPD4164K | 600V/2A | HDIP30 | 3.0V (Ic=1A) | 2.5V (IF=1A) | ~ | _ | - | ~ | ~ | ~ | ~ |
| TPD4164F | 600V/2A | HSSOP31 | 3.0V (Ic=1A) | 2.5V (IF=1A) | ~ | _ | _ | ~ | ~ | ~ | ~ |
| TPD4165K | 600V/3A | HDIP30 | 2.6V (Ic=1.5A) | 1.9V (IF=1.5A) | ~ | _ | _ | ~ | ~ | ~ | \checkmark |

Table 1.2.2 Product example of motor control IC with sine-wave PWM control

| | | | Position sensing | Function | | | | | | | | | | | | | | | | | | |
|----------------------------|---------|----------------------|--|-----------------------------|------------------------|-------------------|------------------|---|------|------|------|------|------|------|------|------|------|--|---|---|---|--------------|
| Product name | Package | V _{CC} / Io | | Lead angle control | Built-in oscillator | Lock detection | Current limit | Other protection function ^(Note 1) | | | | | | | | | | | | | | |
| TB6551FAG | SSOP24 | 12V/2mA | Hall effect | External setting | - | - | ~ | \checkmark | | | | | | | | | | | | | | |
| TB6556FG | SSOP30 | 12V/2mA | IC | | - | - | \checkmark | \checkmark | | | | | | | | | | | | | | |
| TB6584FNG/AFNG (Note 2) | SSOP30 | 18V/2mA | | Current Feedback | ~ | - | ~ | ~ | | | | | | | | | | | | | | |
| TB6634FNG | SSOP30 | 18V/2mA | Hall element or Hall effect IC | Hall | Hall | Hall | Hall | Hall | Hall | Hall | Hall | Hall | Hall | Hall | Hall | Hall | Hall | | ~ | ~ | ~ | \checkmark |
| TB6631FNG | SSOP30 | 18V/2mA | | RPM Feedback (Note 3) | ~ | _ | ~ | ✓ | | | | | | | | | | | | | | |
| TC78B041FNG | SSOP30 | 18V/2mA | | Intelligent | ✓ | ✓ | ~ | ✓ | | | | | | | | | | | | | | |
| TC78B042FTG | QFN32 | 18V/2mA | | Phase Control (Note4) | ~ | ~ | ~ | ✓ | | | | | | | | | | | | | | |

Note 1: Including gate block protection, position signal abnormality protection and VCC undervoltage protection

- Note 2: Specifications such as modulation generation method and automatic advance angle mode differ. Refer to the data sheet of each product for details.
- Note 3: Internal auto lead angle control based on the frequency of the FG signal.
- Note 4: Toshiba's original automatic phase adjustment function.

 Table 1.2.3 Product example of microcontroller with sine-wave PWM control

| | | | Max | | Operating Voltage (V) | |
|--------------|---------|---------------------|---------------------|---------------------------------|-----------------------|-----|
| Product name | Package | ROM size (Bytes) | RAM size (Bytes) | operating frequency (MHz) | Min | Max |
| TMPM375FSDMG | SSOP30 | 64K | 4K | 40 (Note 1) | 4.5 | 5.5 |
| TMPM372FWUG | LQFP64 | | | | | |
| TMPM373FWDUG | LQFP48 | 128K | 6K | 30 (Note 1) | 4.5 | 5.5 |
| TMPM374FWUG | LQFP44 | | | 52 | | |
| TMPM370FYDFG | QFP100 | | 10/ | (Note 2) | 4 5 | |
| TMPM370FYFG | LQFP100 | 250K | IUK | 80 () | 4.5 | 5.5 |
| TMPM376FDDFG | QFP100 | E10V | 221/ | OO (Note2) | 4 5 | |
| TMPM376FDFG | LQFP100 | 512K | 32K | 80 (1997) | 4.0 | 5.5 |

Note 1: Ambient temperature -40 °C to 105 °C

Note 2: Ambient temperature -40 °C to 85 °C



1.3. Block diagram



Figure 1.3.1 Block diagram for TPD4163K/TPD4164K/TPD4165K



Figure 1.3.2 Block diagram for TPD4163F/TPD4164F

Metal heat dissipation surface : Heat dissipation can be improved by attaching to the heatsink. The metal surface has the same potential as GND pin. When it is necessary to insulate, insert an insulating sheet or the like

between heat sink and package surface.

2. Package information

Two types of packaging are available: HDIP30 (lead insert type) and HSSOP31 (surface mount type). Select the package according to the application, mounting method of the board, etc.

2.1. HDIP30

HDIP30 package has high voltage power pins and control pins separated on both sides of the package, making it easier to design the PCB. In addition, while the package thickness has been made thinner, a wide pin-to-pin distance is ensured for high voltage pins.

Metal heat dissipation surface is exposed on the package surface, and heat dissipation can be improved by attaching the heatsink. HDIP30 package supports to mount by flow and soldering iron.



Figure 2.1.1 HDIP30 packege

2.1.1. Package dimensions

Package Code: P-HDIP30-1233-1.78-001



Figure 2.1.2 Dimensions of HDIP30 package

Unit: mm





2.1.2. Marking





2.1.3. PCB land pattern dimensions (Reference)





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2.1.4. Attaching a heatsink

A heatsink may be required, depending on the ambient temperature or the heating of the HVIPD or its neighboring devices. Attach a heatsink as described below if necessary.

• Applying of silicon grease

Contact thermal resistance is improved by applying silicon grease between device and heat sink. Please put a light coat and uniform of silicon grease. Nonvolatile silicon grease is recommendable. There is the possibility that volatile one have a cracking of grease and a change for the worse of heat radiation effect when use for a long time.

• Tightening torque

It has the possibility to break the screw thread/hole or give damage of strain with excessive tightening torque. When over some tightening torque point, contact thermal resistance became saturated. Following table is the recommendation of tightening torque to avoid the device stress with optimum contact thermal resistance. Carry out a temporary bundle if needed.

 Table 2.1.1 Recommended Screw, tightening torque and Maximum tightening torque

| Recommended | Recommended tightening | Maximum tightening |
|-------------|------------------------|--------------------|
| Screw | torque | torque |
| M2.6 | 0.5 N∙m | 0.6 N∙m |

• Flatness of the surface

The surface where the device is attached must be sufficiently smooth. Warps, large bumps or hollows in the surface, or foreign bodies such as punching burrs or chips lodged between the device and the attachment face can cause devise failure in the worst case. To avoid these problems, the flatness of the surface where the device is attached should be within 50 μ m.



Figure 2.1.5 Flatness of the surface

Handling precautions

•This product has a MOS structure and is sensitive to electrostatic discharge. When handling this product, ensure that the environment is protected against electrostatic discharge.

•Package have an exposed metal portion on the same side mold surface of marking area. This portion is at the same potential as product GND pin (1/18 pin) .As necessary, please make safety provisions for insulation between package and heat sink.





Figure 2.1.6 The example of heatsink attachment

2.2. HSSOP31

HSSOP31 package has high voltage power pins and control pins separated on both sides of the package, making it easier to design the PCB. In addition, the package thickness has been made thinner, and the size has been made smaller.

Metal heat dissipation surface is exposed on the package surface, and heat dissipation can be improved by attaching the heatsink. HSSOP31 package supports to mount by reflow and soldering iron.

2.2.1. Package dimensions

Package Code: P-HSSOP31-0918-0.80-002



Figure 2.2.1 Dimensions of HSSOP31 package



2.2.2. Marking



Figure 2.2.2 Part marking on HDIP31 package

2.2.3. PCB land pattern dimensions (Reference)



Figure 2.2.3 Land pattern of HSSOP31 package (Reference)

2.2.4. Attaching a heatsink

A heatsink may be required, depending on the ambient temperature or the heating of the HVIPD or its neighboring devices. Attach a heatsink as described below if necessary.

Heatsink attachment example

(1) Example of using an insulating sheet





(2) Example of using resin or gelatinous insulating material



Figure 2.2.5 Heatsink attachment example (using resin or gelatinous insulating material)

(3) Example of other heatsink attachment method



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• Mounting to substrate

Where the HSSOP31 package is sandwiched between the heat sink and the substrate, it the static load should be no greater than 10N. The load should be spread uniformly across the device, and screw mountings should not result in substrate bending as shown in right Figure, as the resulting distortion **F** could cause device damage or failure. Consider using spacers or equivalent to attach the heat sink so as to prevent substrate bending.



Figure 2.2.9 Bent PCB

• Flatness

The surface beneath the heat sink to which the device is attached must be suitably smooth and flat. The heat sink should likewise show no signs of warping or undulation and should be free of foreign matter such as burrs and scraps from pressing and cutting processes. In the worst case scenario this could lead to device failure. And heat fins fixed to the top of the package can cause device failure due to heat stress. Hard components (such as the heat sink) should be mounted onto the package together with a buffer layer (typically soft insulating sheet or conductive gel). Silicon grease should be avoided.

3. Pin description

3.1. Pin assignment

| Pin No. | | | |
|----------------------------------|-----------------------|------------------|---|
| TPD4163K TPD4164K TPD4165K | TPD4163F TPD4164F | Symbol | Pin Description |
| 1/18 | 11 | GND | Ground pin. |
| 2/9/11/13/ 15/26/29 | 12/13/15/ 17/19/23 | NC * | Unused pin, which is not connected to the chip internally. |
| 3 | 29 | HU | The control terminal of IGBT by the high side of U. It turns off less than 1.5 V. It turns on more than 2.5 V. |
| 4 | 28 | ΗV | The control terminal of IGBT by the high side of V. It turns off less than 1.5 V. It turns on more than 2.5 V. |
| 5 | 27 | HW | The control terminal of IGBT by the high side of W. It turns off less than 1.5 V. It turns on more than 2.5 V. |
| 6 | 26 | LU | The control terminal of IGBT by the low side of U. It turns off less than 1.5 V. It turns on more than 2.5 V. |
| 7 | 25 | LV | The control terminal of IGBT by the low side of V. It turns off less than 1.5 V. It turns on more than 2.5 V. |
| 8 | 24 | LW | The control terminal of IGBT by the low side of W. It turns off less than 1.5 V. It turns on more than 2.5 V. |
| 10 | 22 | SD | Input pin of external protection. ("L" active, It doesn't have hysteresis.) |
| 12 | 20 | RS | Over current detection pin. |
| 14 | 18 | DIAG | With the diagnostic output terminal of open drain, a pull-up is carried out by resistance. It turns on at the time of unusual. |
| 16 | 16 | V _{CC} | Control power supply pin. (15 V typ.) |
| 17 | 14 | V _{REG} | 5 V regulator output pin. |
| 19 | 10 | IS1 | U-phase IGBT emitter and FRD anode pin. |
| 20 | 9 | IS2 | V-phase IGBT emitter and FRD anode pin. |
| 21 | 8 | U | U-phase output pin. |
| 22 | 7 | BSU | U-phase bootstrap capacitor connecting pin. |
| 23 | 6 | BSV | V-phase bootstrap capacitor connecting pin. |
| 24 | 5 | V | V-phase output pin. |
| 25 | 4 | V _{BB} | High-voltage power supply input pin. |
| 27 | 3 | BSW | Unused pin, which is not connected to the chip internally. |
| 28 | 2 | W | W-phase bootstrap capacitor connecting pin. |
| 30 | 1 | IS3 | W-phase output pin. |

Table 3.1.1 Pin description

*NC pins are unused pins and are not connected to the chip internally. Although the electrical characteristics are not affected, it is recommended that the pins be soldered to the board.



Figure 3.1.1 HDIP30 pin assignment (TPD4163K/TPD4164K/TPD4165K)



Figure 3.1.2 HSSOP31 pin assignment (TPD4163F/TPD4164F)

4. Usage considerations and functional descriptions

4.1. Application circuit example

The pin numbers in the figure indicate the number of TPD4163K, TPD4164K and TPD4165K.









The table below lists the standard external parts.

| | | | | aluc |
|--|----------------------|--|-----------------------------|---------|
| Parts | Reference value | | Purpose | Remarks |
| C ₁ , C ₂ , C ₃ | | 25 V/2.2 μF | Bootstrap capacitor | (1) |
| C4 | | 25 V/10 μF | VCC power supply stability | (2) |
| C5 | | 25 V/0.1 μF | VCC for surge absorber | (2) |
| C ₆ | | 25 V/10 μF | VREG power supply stability | (3) |
| C ₇ | | 25 V/0.1 μF | VREG for surge absorber | (3) |
| R_1 | | 5.1 kΩ | DIAG pin pull-up resistor | (4) |
| R ₂ | | 10 kΩ | SD pin pull-up resistor | (5) |
| | TPD4163F TPD4163K | 0.62 Ω ± 1 % (1 W) | | |
| R ₃ | TPD4164F TPD4164K | $0.35 \ \Omega \ \pm \ 1 \ \% \ (1 \ W)$ | Overcurrent detection | (6) |
| | TPD4165K | 0.2 Ω ± 1 % (2 W) | | |

 Table 4.1.1
 Application circuit example: External parts value

(1) BSU, BSV and BSW pin

Connect the bootstrapped capacitor C1, C2 and C3 between BSU and U pin, between BSV and V pin, and between BSW and W pin, respectively. These pins are used to power the internal circuit that drives the high-side IGBT. The required capacity of the bootstrap capacitor depends on the drive conditions of the motor. 5V (typ.) is applied to the capacitor. Refer to the calculation formula and select a capacitor with sufficient derating considerations.

| Item | Parts No | Parts | Reference value |
|---|------------|--|-----------------|
| Between BSU and U Between BSV and V Between BSW and W | C1, C2, C3 | Ceramic capacitors Electrolytic capacitor | 25 V / 2.2µF |

 Table 4.1.2
 BSU, BSV and BSW pin capacitor

Calculating the value of the bootstrap capacitor required

Smaller capacitance among CB(ON) and CB(OFF) is the required capacitance.

CB(ON)=IBS(ON) x High-side IGBT on-time (max) / (5 + VF (FRD) - VBSUVD) [F] CB(OFF)=IBS(OFF) x Low-side IGBT off-time (max) / (5 +VF (FRD) - V_{BS}UVD) [F] CB: Minimum capacitance of the bootstrap capacitor IBS(ON) : Maximum Bootstrap Current dissipation in high side ON (150 μ s) IBS(OFF) : Maximum Bootstrap Current dissipation in high side OFF(140 μ s) VF (FRD) : Forward voltage of the flywheel diode (V_FH or V_FL) V_{BS}UVD : Maximum V_{BS} under voltage protection (4V)

(2) V_{cc} pin

Connect the ceramic capacitor and the electrolytic capacitor between Vcc and SGND/PGND as close to the IC as possible if needed in order to reduce the noise and the fluctuation of the voltage at Vcc terminal. In particular, the power supply fluctuations and the noise, which generate at high frequency, can be effectively reduced by connecting ceramic capacitors near the IC.

If you need to increase the noise tolerance of VCC lines, add a Zener Diode between VCC-GND as needed.

| Item | Parts No | Parts | Reference value |
|---------------------|----------|------------------------|-----------------|
| Botwoon Var and CND | C4 | Electrolytic capacitor | 25 V / 10µF |
| | C5 | Ceramic capacitor | 25 V / 0.1µF |

Table 4.1.3Vcc pin Connecting Capacitors

(3) V_{REG} pin

 V_{REG} pin is output pin of 5V voltage regulator. It can be used for power supply for pull-up resistor of DIAG pin, pin setting, and power supply of peripheral IC. At that time, the output current can be used within 30mA (max). To prevent oscillation, add a capacitor to VREG terminal. In addition, connect a capacitor as close to IC as possible between VREG and GND to minimize noise and fluctuations on VREG terminals.

 Table 4.1.4
 V_{REG} pin Connecting Capacitors

| Itom | Darta No | Parta | Deference value |
|----------------------|----------|------------------------|-----------------|
| Item | Parts NO | Parts | Reference value |
| Between Vara and CND | C6 | Electrolytic capacitor | 25 V / 10µF |
| Detween VREG and GND | C7 | Ceramic capacitor | 25 V / 0.1µF |

| Table 4.1.5 | Regulator Voltage (Condition: V _{CC} =15V, I _{REG} =30mA) Unit: V |
|-------------|---|
|-------------|---|

| Characteristic | Symbol | Min | Тур. | Max |
|-------------------|------------------|-----|------|-----|
| Regulator voltage | V_{REG} | 4.5 | 5 | 5.5 |

(4) DIAG pin

DIAG pin is open-drain output-type pin. To use this pin as High/Low level output-signal, connect a pull-up resistor to the external power supply or V_{REG} pin. When the output MOSFET of DIAG pin is turned ON with a pull-up resistor connected, the voltage of the pin is set to L level. When it is turned OFF, the voltage of the pin is set to H level. When pulling up to VREG pin, it is recommended that the resistor be connected between 1 k Ω and 10 k Ω . When using a pull-up resistor for an external power supply, select a pull-up power supply voltage and resistor so that the output voltage 20V and output current 20mA of the absolute maximum rating are not exceeded.

When DIAG pin is not used, connect it to GND.

| | 5 | | | | |
|----------------------------------|----------------|----------|-----------------|-------------------|--|
| ltem | Parts No | Parts | Reference value | Recommended range | |
| Between DIAG and power supply | R ₁ | Resistor | 5.1kΩ | 1kΩ to 10kΩ | |

Table 4.1.6 DIAG Pin Connecting Resistor

(5) SD pin

By inputting Low level to SD pin, IGBTs of the U, V, and W-phase high-side and low-side can be switched all-off.

High/Low level of SD pin is detected using the input-voltage 2.5V (typ.) as the threshold. When connecting to an external circuit to input a signal, it is recommended to connect a pullup resistor of $5k\Omega$ to $15k\Omega$ to VREG pin to prevent malfunction due to noise-induced effects. When SD pin is fixed at High level, it is recommended to short-circuit VREG pin and SD pin.

| ltem | Parts No | Parts | Reference value | Recommended range | |
|--|----------|----------|-----------------|-------------------|--|
| Pull-up resistor between SD and V_{REG} | R2 | Resistor | 10kΩ | 5kΩ to 15kΩ | |

Table 4.1.7SD Pin Connecting Resistor

(6) Resistor for connecting IS1, IS2 and IS3 pins and RS pin

Design IS1/IS2/IS3 terminals to be connected to the shunt resistor as short as possible to avoid malfunction and damage. Add a surge-protecting diode between IS1/IS2/IS3 terminal-GND terminals for longer wire lengths. Motor current flows through IS1, IS2 and IS3 terminals. Wire the terminals in a wider pattern.

As shown in Fig. 4.1.1, when using the overcurrent protection function with the 1-shunt resistor detection method, short-circuit IS1, IS2, IS3 pin and RS pin, connect a detection resistor between GND, and set the detection current of the overcurrent protection.

The relation between the over-current protection detection current I_0 and the detection resistor R_1 is roughly calculated by the following formula.

 $I_O = V_R \! / \ R_3$

Overcurrent Protective Operating Voltage V_R : 0.46V (Min), 0.5 V (Typ.), 0.54V (Max)

e.g.) If R₃ resistor is set to 0.51 Ω , I_{OU} (typ.) = 0.5 V (typ.)/0.51 $\Omega \simeq 0.98$ A Note that a large current flows through the detector resistor R₃, so pay careful attention to the ratings of the external components when selecting with margins. During operation, the power P across the sense resistor is calculated as maximum P=0.525Vx0.525V/ R₃. For example, when R₃=0.51 Ω , P=0.54W, so use a resistance higher than 1 W for the rated power.

| ltem | Parts No | Parts | Reference value | Reference value |
|--|----------|----------|----------------------|--|
| Current sensing resistor between IS1/IS2/IS3 and GND | R3 | Resistor | TPD4163F TPD4163K | $0.62 \ \Omega \pm 1 \% (1 \text{ W})$ |
| | | | TPD4164F TPD4164K | $0.35 \ \Omega \ \pm \ 1 \ \% \ (1 \ W)$ |
| | | | TPD4165K | 0.2 Ω ± 1 % (2 W) |

Table 4.1.8Current Detection Resistor(When Using the Overcurrent Protection Function of the Product)

To use the overcurrent protection function of the control IC or MCU as shown in Fig. 4.1.2, short-circuit RS pin to GND. Also, if noise is affected by the routing of the wires from the current detecting resistor across IS1/IS2/IS3-GND to the control IC or MCU, consider measures such as adding a low-pass filter to remove noise as needed.

(7) HU, HV, HW, LU, LV and LW pin

HU, HV, HW, LU, LV and LW pins control the on/off status of the U-, V-, and W-phase high-side and low-side IGBT. HU controls U-phase high side, HV controls V-phase high side, HW controls W-phase high side, LU controls U-phase low side, LV controls V-phase low side, and LW controls W-phase low side. Connect it to a control IC or microcontroller that generates three-phase brushless motor control signals.

(8) U, V and W pin

Connect each pin to the coil of the three-phase brushless motor. The motor current flows through each pin, so the wiring pattern should be wide.

(9) V_{BB} pin

 V_{BB} pin is a high-voltage power supply pin and connected to the collector of the high-side IGBT. Take measures such as adding a capacitor between V_{BB} and GND so that the operating power supply 450V is not exceeded when the motor is stopped or during operation. Motor



current flows through V_{BB} pin. Wire the pin in a wider pattern.

(10) GND pin

Design the circuit so that there is no path through which the motor current flows in the wire connecting GND terminal and the overcurrent detecting resistor. Also design the circuit so that the wires connecting HVIPD's GND pin to the control IC or MCU's GND pin do not flow the motor current.

4.2. Protection function

Under voltage protection

The HVIPD incorporates an under voltage protection circuit, which prevents internal IGBTs from operating in an unsaturated region when the VCC and VBS voltages drop.

When VCC drops to VCCUVD (= 11V typ.), all the IGBT outputs shut down regardless of the input states. Under voltage protection has a hysteresis of 0.5V. When VCC rises back to VCCUVR (= 11.5V typ.), the MOSFETs return to normal operation and turn on according to the input states. When VCC under voltage protection is tripped, the DIAG output toggles its state. However, the DIAG output might remain unchanged if VCC is lower than 7V. (All the IGBT outputs shut down when VCC drops below 11V, even if the DIAG output does not toggle.)



Figure 4.2.1 V_{cc} undervoltage protection operation

When VBS drops to VBSUVD (= 3V typ.), all the high-side IGBT outputs shut down. When VBS rises back to VBSUVR (= 3.5V typ.), 0.5V higher than VBSUVD, the high-side IGBTs return to normal operation and operate according to the control signals. VBS under voltage protection does not cause the DIAG output to toggle.





Figure 4.2.2 V_{BS} undervoltage protection operation

Overcurrent protection

The HVIPD incorporates the overcurrent protection circuit, which protects itself from excessive current at motor startup or when the rotor is locked. This protection function detects the voltage generated in the current-sensing resistor connected to the RS pin. When this voltage exceeds V_R (= 0.5V typ.), the IGBT outputs temporarily shut down after a delay of 2µs (typ.) to prevent a further increase in current. Setting the control signals to all-Lows releases the HVIPD from the shutdown state.

Selecting the overcurrent resistor:

 $R_3 = V_R \div I_0$

 V_{R} : Overcurrent voltage, I_{O} : Overcurrent, R_{3} : Overcurrent resistor

| Characteristics | Symbol | Min | Тур. | Max |
|-----------------------------------|----------------|------|------|------|
| Overcurrent protection voltage | V _R | 0.46 | 0.5 | 0.54 |

Table 4.2.1 Overcurrent protection voltage Unit: V

Setting the overcurrent protection delay time

The HVIPD incorporates the filter into RS pin to prevent the current limiter from malfunctioning because of the noise at the overcurrent-sensing resistor. The delay time from when the overcurrent senses a current exceeding the overcurrent to when the IGBTs outputs shut down is determined by the sum of the filtering time (dead time) of the filter and the delay time of the control circuit:

Overcurrent protection delay time (D_t) = filtering time (dead time) + control circuit delay

If the overcurrent resistor has large noise, the dead time of the internal filter may be insufficient. In that case, an external filter should be added to RS pin. Note that an external filter increases the current-limiting delay time (i.e., the time required for the IGBT outputs to shut down).



Table 4.2.2 Over current protection delay time Unit: µs

Figure 4.2.3 Overcurrent protection operation

Thermal shutdown

The HVIPD incorporates the thermal shutdown circuit to protect itself from excessive temperature. When an external factor or internally generated heat causes the chip temperature to rise to the thermal shutdown temperature (TSD), all the IGBT outputs shut down regardless of the input states. Thermal shutdown has a hysteresis (Δ TSD) of 50°C typical. When the chip temperature drops below (TSD – Δ TSD), the MOSFETs return to normal operation and turn on according to the input states.

The HVIPD senses its chip temperature at one position. Suppose that IGBTs are heat sources. The time taken to shut down the IGBTs differs, depending on the distance between a heat source and the temperature sensor. Therefore, the chip temperature may be higher than the thermal shutdown temperature (TSD) when the thermal shutdown circuit is tripped.





Figure 4.2.4 Thermal shutdown operation

SD function

The overcurrent condition may be detected by an external circuit. Setting the SD pin Low causes all the IGBT outputs to turn off after a delay of 2µs (typ.). Setting all control signals to low level releases the IGBT outputs from shutdown mode.





4.3. Power supply sequencing

We do not recommend the following power sequences:

At power-on: Powering on V_{CC} after V_{BB} and control signals

At power-off: Powering off V_{CC} before V_{BB} and control signals

| A | <u> </u> | | |
|-----------------|-----------------|-----------------|--------------|
| 1 | 2 | 3 | • / ^ |
| V_{CC} | V_{BB} | Control signals | \checkmark |
| V_{CC} | Control signals | V _{BB} | \checkmark |
| V_{BB} | V_{CC} | Control signals | \checkmark |
| V_{BB} | Control signals | V _{CC} | × |
| Control signals | V_{CC} | V _{BB} | \checkmark |
| Control signals | V_{BB} | V_{CC} | х |

Table 4.3.1 At power-on

| A | <u> </u> | | |
|-----------------|-----------------|-----------------|--------------|
| 1 | 2 | 3 | • / ^ |
| V _{CC} | V_{BB} | Control signals | × |
| V _{CC} | Control signals | V_{BB} | × |
| V _{BB} | V_{CC} | Control signals | \checkmark |
| V_{BB} | Control signals | V _{CC} | \checkmark |
| Control signals | V_{CC} | V_{BB} | \checkmark |
| Control signals | V _{BB} | V _{CC} | ✓ |

Table 4.3.1 At power-off

 $\checkmark: \mathsf{Recommended}, \, \times: \, \mathsf{Unrecommended}$

Note that even when V_{CC} and V_{BB} are powered off, the device might be permanently damaged if the V_{BB} line is disconnected by a relay or other means while the motor is running because this blocks a current recirculation path to V_{BB} .

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4.4. Calculating power losses

This section shows how to calculate power losses that occur when the output current is sinusoidal.

 $P = P_{on} + P_t + P_{iBB} + P_{iCC}$

(1) Conduction loss: Pon

 $P_{on} = P_{H} + P_{L} + P_{D} (W)$

- + High-side IGBT conduction loss: P $_{\rm H}$ = I \times V $_{satH}$ \times (1/8 + D/3 π \times COS $\theta)$ \times 3
- Low-side IGBT conduction loss: $P_{L}=I \times V_{satL} \times (1/8 + D/3\pi \times COS\theta) \times 3$
- + Flywheel diode conduction loss: P $_{D}$ = I \times V $_{F}$ \times (1/8–D/3п \times COS0) \times 6
 - I_{p} : Peak motor winding current (A)
 - $V_{\text{satH}}/V_{\text{satL}}$: Output saturation voltage (V)
 - V_F : Forward voltage drop of the FRD (V)
 - D : PWM duty cycle
 - θ : Power factor
- (2) MOSFET switching loss: P_t

 $P_{t} = (W_{ton} + W_{toff}) \times f_{C} / \pi \times 6 (W)$ $W_{ton} : Turn-on loss (\mu J per pulse)$ $W_{toff} : Turn-off loss (\mu J per pulse)$ $f_{C} : PWM switching frequency (Hz)$

- (3) V_{BB} power consumption: P_{iBB} (W)
 - $\mathsf{P}_{\mathsf{iBB}} = \mathsf{V}_{\mathsf{BB}} \times \, \mathsf{I}_{\mathsf{BB}} \, (\mathsf{W})$

 I_{BB} : V_{BB} supply current (A) $\,*$ Supply current when all phases are off

- (4) V_{CC} power consumption: P_{iCC}
 - $P_{iCC} = V_{CC} \times I_{CC} (W)$

 I_{CC} : V_{CC} supply current (A) * Supply current during normal operation





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