

# Basic Electrical Characteristics and Application Circuit Design of Photovoltaic Couplers for MOSFET Drive for Relays

**Outline:**

Photovoltaic-output photocouplers(photovoltaic couplers), which incorporate a photodiode array as an output device, are commonly used in combination with a discrete MOSFET(s) to form a semiconductor relay. This application note discusses the electrical characteristics and application circuits of photovoltaic-output photocouplers.

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Typically, photocouplers consist of a light emitting device optically coupled with a light detecting device via a transparent galvanic insulator. They are commonly used to transfer an electrical signal between two circuits with different ground potentials by means of light. In the past, electromagnetic relays, isolation transformers, and other devices were used to transfer electrical signals from an integrated circuit or between isolated primary and secondary sides. At present, photocouplers are generally used because they help resolve an impedance mismatch, provide higher isolation between input and output, suppress induced electromotive force, and simplify noise blocking. A photovoltaic-output photocoupler generates electricity on its own in response to light energy from the input light emitting diode (LED). Capable of driving a discrete MOSFET(s) without a power supply, photovoltaic-output photocouplers are expected to replace conventional mechanical relays. This application note provides a description of their electrical characteristics and application circuits for engineers who are unfamiliar with photovoltaic-output photocouplers.

### 1. What is a photovoltaic-output photocoupler?

#### 1.1 Structure of a photovoltaic-output photocoupler

As is the case with other types of photocouplers, photovoltaic-output photocouplers consist of an input light emitting device optically coupled with an output light detecting device via a transparent galvanic insulator (Figure 1.1(a)). In the case of photovoltaic-output photocouplers, an infrared LED is used as a light emitting device whereas a photodiode array is used as a light detecting device (Figure 1.1(b)).

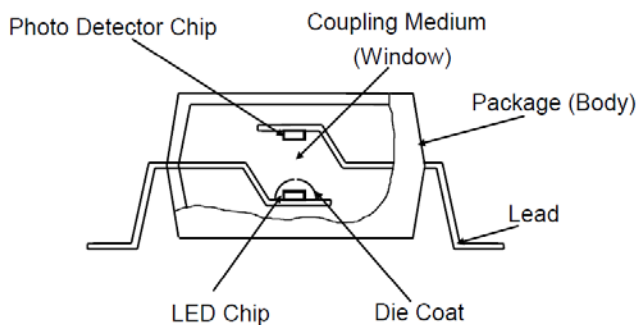


Figure 1.1(a) Internal structure example

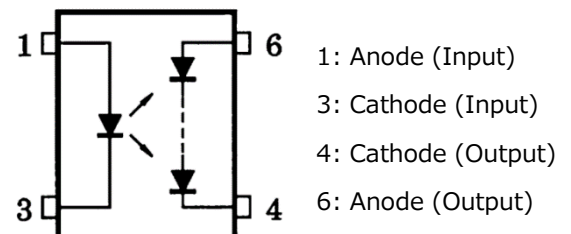


Figure 1.1(b) Pin assignment example

#### 1.2 Principle of operation of a photovoltaic-output photocoupler

A photodiode that detects light in the photovoltaic-output photocoupler is a semiconductor device with a pn junction.

When a photodiode detects light with energy greater than its energy band gap ( $E_g$ ), the excited electrons move to the n region (holes move to the p region), causing the number of electrons in the n region and the number of holes in the p region to increase. This creates a difference in potential between the n and p regions, with the n region being positive with respect to the p region. Consequently, a positive open voltage appears in the p region (anode) when both ends of the photodiode are open-circuited whereas short-circuit current

flows from the p region (anode) to the n region (cathode) when they are short-circuited (Figure 1.2). The voltage that appears across a single photodiode is a fraction of a volt. An open voltage of a few volts can be obtained by using an array of photodiodes.

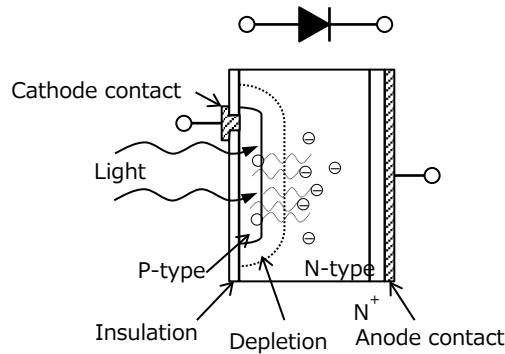


Figure 1.2 Principle of voltage generation in a photodiode

### 1.3 Basic usage of photovoltaic-output photocouplers

A photovoltaic-output photocoupler (PV) generates DC voltage that is used to drive the gate of the following MOSFET(s). Since the short-circuit current from a photovoltaic-output photocoupler is typically on the order of ten to a few tens of microamperes, it is unsuitable for switching power supply drive and other high-speed switching applications. Therefore, photovoltaic-output photocouplers are commonly used for relay applications that tolerate low-speed switching. Photovoltaic-output photocouplers provide an open voltage ( $V_{OC}$ ) of about 7 to 9 V at a room temperature of 25°C. However,  $V_{OC}$  decreases as temperature increases. Therefore, multiple photovoltaic-output photocouplers might be necessary, depending on the environmental conditions under which they are used or the gate threshold voltage ( $V_{th}$ ) of the driven MOSFETs (Figure 1.3(1b)). Discrete MOSFETs contain a parasitic body diode. Therefore, in the case of AC relay applications, it is necessary to connect the drain and source terminals of two MOSFETs as shown in Figure 1.3(1a) (i.e., the drain (source) terminal of a MOSFET and the source (drain) terminal of an adjacent MOSFET). In contrast, in the case of DC relay applications, a single MOSFET suffices as shown in Figure 1.3(2).

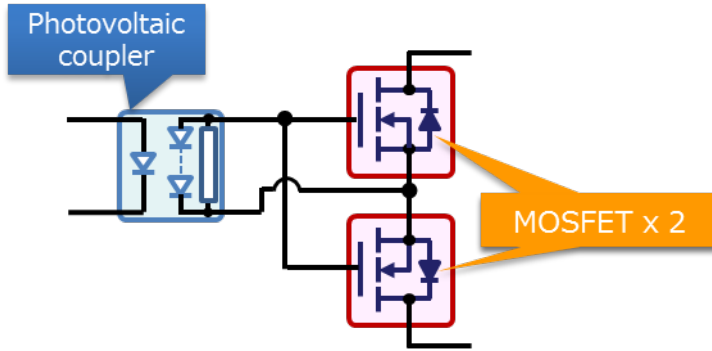


Figure 1.3(1a) AC relay consisting of one PV and two MOSFETs

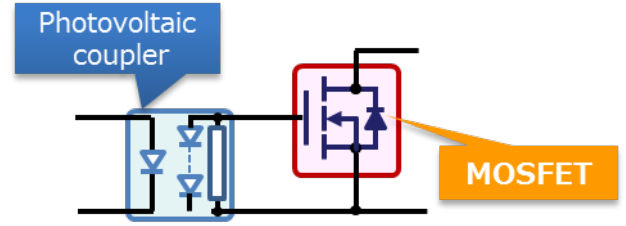


Figure 1.3(2) DC relay consisting of one PV and one MOSFET

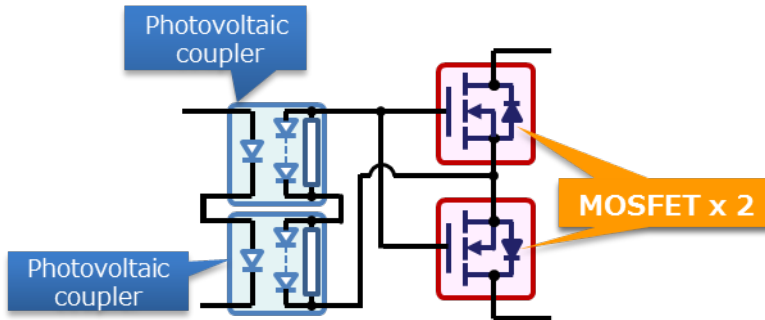


Figure 1.3(1b) AC relay consisting of two PVs and two MOSFETs

A photorelay integrates a photovoltaic-output photocoupler and MOSFETs in a single package. It requires much less board space than a combination of a photovoltaic-output photocoupler and discrete MOSFETs. A disadvantage of the photorelay is that its current rating is constrained by the size of the chips that can be integrated in one package.

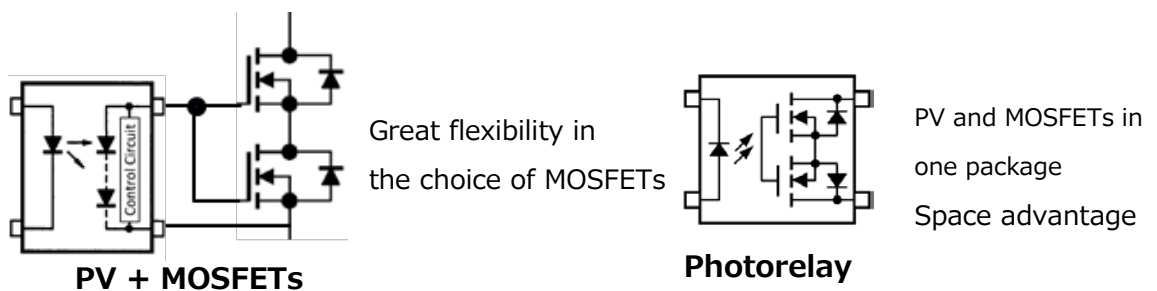


Figure 1.4 PV+MOSFETs vs. photorelay

### 1.4 Advantages of PV+MOSFET combinations

A PV+MOSFET combination compares unfavorably with a conventional mechanical relay in terms of price and has a limit on the maximum power that can be switched. Nonetheless, PV+MOSFET combinations have several advantages over mechanical relays.

### (1) Bounceless switching

A mechanical relay has a physical contact. When the contact opens, it is susceptible to bounce noise, which might affect the correct operation of the neighboring devices (Figure 1.5 (a)).

In contrast, semiconductor relays including PV+MOSFET combinations are free from bounce noise because they have no mechanical parts (Figure 1.5(b)).

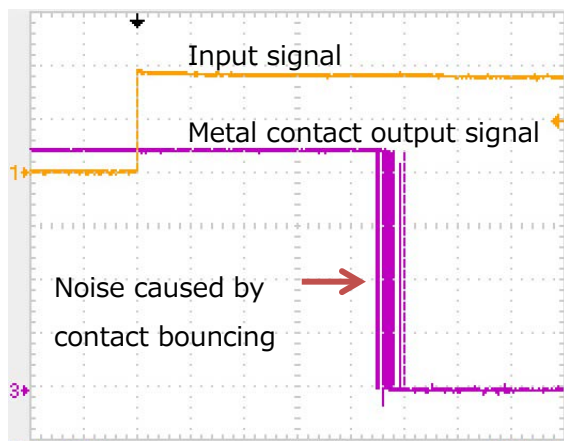


Figure 1.5(a) Operating waveforms of a mechanical relay with a resistive load

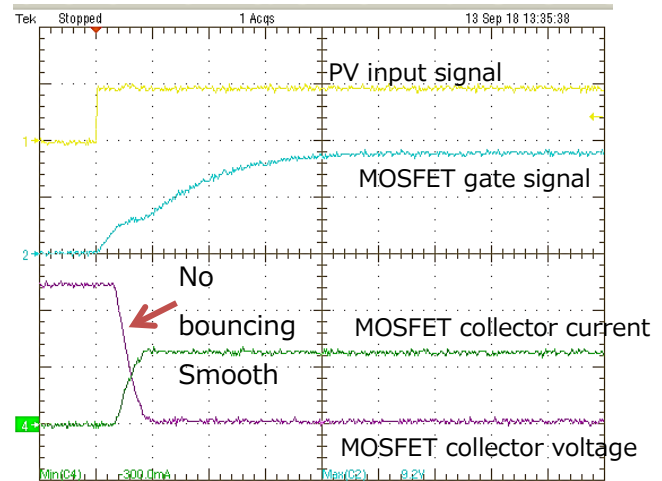


Figure 1.5(b) Operating waveforms of a PV+MOSFET relay with a resistive load

### (2) No limit on the number of contact open/close cycles

Mechanical relays have a limit on the number of open/close cycles because of the use of a mechanical contact. In contrast, semiconductor relays such as PV+MOSFET combinations are free from mechanical aging and failure.

### (3) High response speed

When response speed is a priority, PV+MOSFET relays can be configured to switch faster than mechanical relays although this advantage depends on the on-resistance and gate capacitance of the driven MOSFET. Therefore, PV+MOSFET relays can be used for phase control applications.

### (4) Reduction in the power consumption of a power supply circuit

Because mechanical relays drive a solenoid coil, they require an input current as high as a few tens of milliamperes. In addition, a separate power supply might be needed for a drive circuit that supplies this input current. In contrast, semiconductor relays such as PV+MOSFET combinations require an input current of only a few to 10 or so milliamperes.

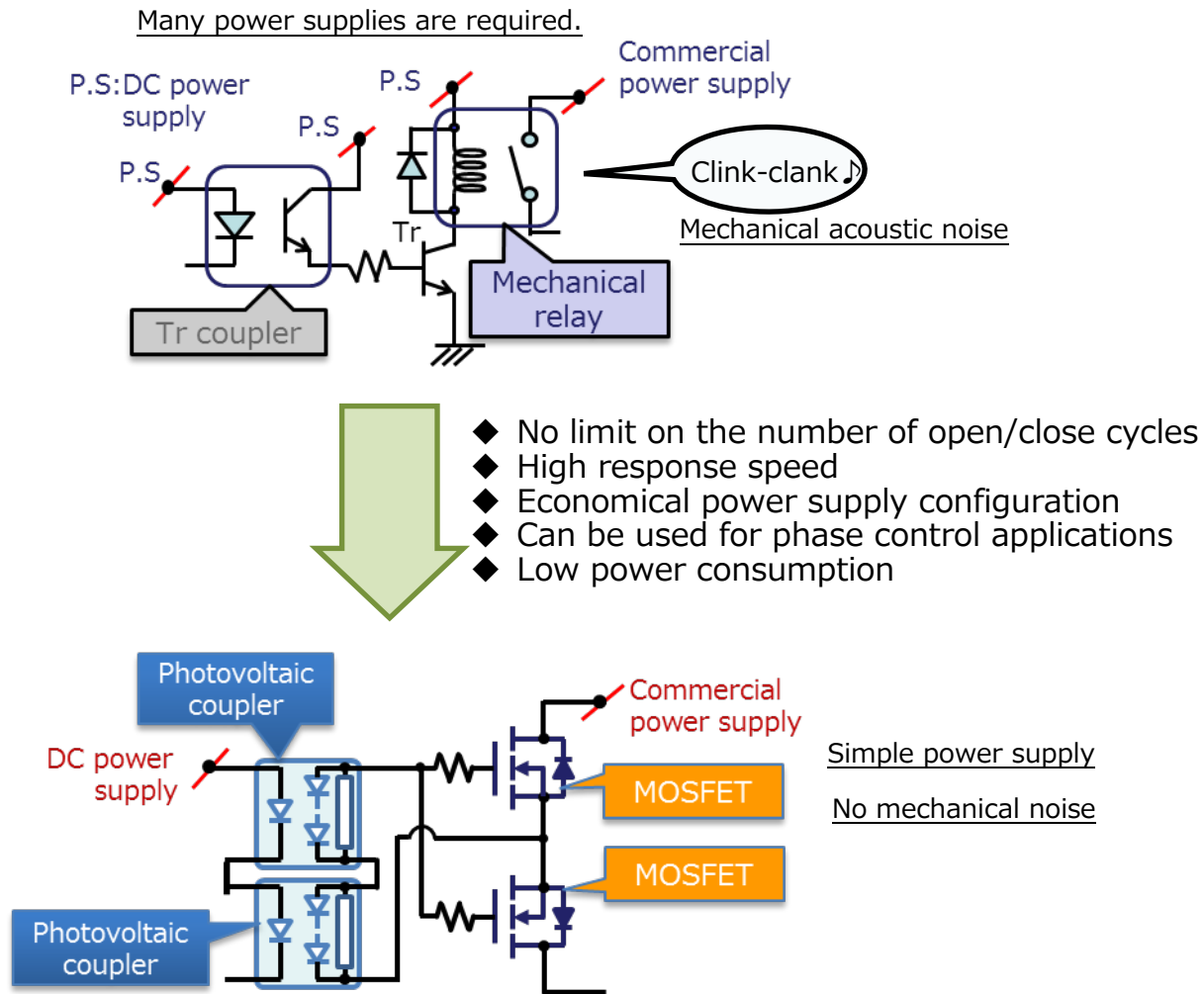


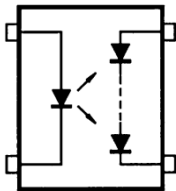
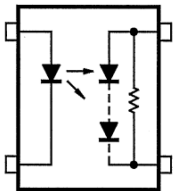
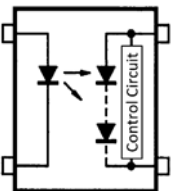
Figure 1.6 Advantages of PV+MOSFETs

### 1.5 Types of photovoltaic-output photocouplers

A photovoltaic-output photocoupler that drives a MOSFET requires a circuit to discharge the gate capacitance to turn it off. Some photovoltaic-output photocouplers incorporate a discharge circuit, and others do not. The simplest photovoltaic-output photocoupler requires an external discharge circuit. In the simplest case, it is a single resistor connected between the anode and cathode outputs of the photovoltaic-output photocoupler. A high-value resistor allows the photovoltaic-output photocoupler to provide an open voltage ( $V_{OC}$ ) close to its  $V_{OC}$  rating. However, a high-value resistor slows the turn-off of a MOSFET because the discharge time is dependent on the product of the gate capacitance of the driven MOSFET and the resistor value ( $C \times R$ ). An advantage of using photovoltaic-output photocouplers without an internal discharge circuit such as the TLP3905 is the flexibility in adjusting open voltage and turn-off time within certain ranges. In contrast, photovoltaic-output photocouplers with an internal discharge circuit such as the TLP191B do not provide such design flexibility, but require fewer parts and less board space and design workload. Another type of photovoltaic-output photocouplers such as the TLP3906 incorporate a discharge clamp circuit instead of a resistor that operates only during the turn-off of a

MOSFET. These photovoltaic-output photocouplers provide the voltage generated by a photodiode array (i.e., open voltage) without attenuation when the LED is on and quickly discharges the MOSFET gate when it turns off. They simplify system design and provide outstanding electro-optical characteristics.

Table 1.1 Types of output circuits in photovoltaic-output photocouplers

Output circuit type	No discharge circuit	Built-in discharge resistor	Built-in discharge circuit
Equivalent circuit			
Product example	TLP3905	TLP191B	TLP3906
Characteristics	<ul style="list-style-type: none"> <li>Requires an external discharge circuit</li> </ul>	<ul style="list-style-type: none"> <li>No need for an external discharge circuit</li> <li>Limited MOSFET gate discharge performance because of the fixed internal resistor value</li> </ul>	<ul style="list-style-type: none"> <li>No need for an external discharge circuit</li> <li>Provides higher MOSFET gate discharge performance and thus shorter MOSFET turn-off time than a built-in resistor</li> </ul>

## 2. Major electrical characteristics and behavior of photovoltaic-output photocouplers

This section describes major electrical performance characteristics shown in the datasheets of photovoltaic-output photocouplers and their behaviors that you need to understand to design a PV+MOSFET relay.



Table 2.1 Major terms used in the technical datasheets of photovoltaic-output photocouplers

Term	Symbol	Description
Input Forward Current	$I_F$	Rated current that can flow continuously in the forward direction of the LED
Input Power Dissipation	$P_D$	Rated power that can be dissipated in the LED
Open Voltage	$V_{OC}$	Output photovoltaic voltage generated at the specified input current, $I_F$
Short-Circuit current	$I_{SC}$	Output photo-current generated by the specified input current, $I_F$
Turn-ON time	$t_{on}$	Time taken for the output waveform to change from 100% to 10% after the LED current is turned on under the specified conditions
Turn-OFF time	$t_{off}$	Time taken for the output waveform to change from 0% to 90% after the LED current is turned off under the specified conditions

### 2.1 $V_{OC}$ - $I_F$ characteristics

The  $V_{OC}$ - $I_F$  characteristics show the dependence of open voltage ( $V_{OC}$ ) on input forward current ( $I_F$ ). As  $I_F$  increases,  $V_{OC}$  increases. In the case of photovoltaic-output photocouplers that require an external discharge resistor such as the TLP3905, a high-value resistor helps maintain  $V_{OC}$  at high voltage as shown in Figure 2.1. However, a high-value resistor causes the MOSFET turn-off time to increase as indicated by the  $t_{off}$ - $C_L$  characteristics of Figure 2.6 shown later. The TLP3906 incorporating a discharge circuit does not require an external resistor. Therefore, Figure 2.2 gives only one  $V_{OC}$  characteristic when its outputs are open-circuited. The TLP3906 incorporates a discharge circuit that provides the highest open voltage and efficiently turns off a MOSFET.

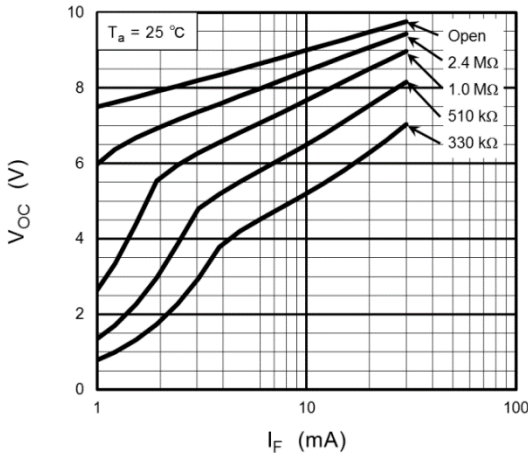


Figure 2.1 TLP3905  $V_{OC}$ - $I_F$  characteristics

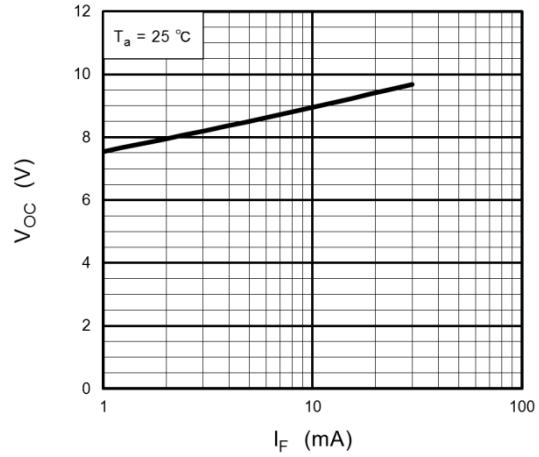


Figure 2.2 TLP3906  $V_{OC}$ - $I_F$  characteristic

2.2  $V_{OC}$ - $T_a$  characteristic

The  $V_{OC}$ - $T_a$  characteristic shows the dependence of open voltage ( $V_{OC}$ ) on the ambient temperature ( $T_a$ ).  $V_{OC}$  decreases as the ambient temperature increases, as shown in Figure 2.3. Even at the highest ambient temperature,  $V_{OC}$  must be higher than the gate threshold voltage ( $V_{th}$ ) of the driven MOSFET. If  $V_{OC}$  is lower than  $V_{th}$ , multiple photovoltaic-output photocouplers must be connected in series in order to obtain a higher open voltage. The  $V_{OC}$ - $T_a$  characteristic is negatively sloped because both the light output of an LED and the open voltage of a photodiode array decrease as the ambient temperature increases.

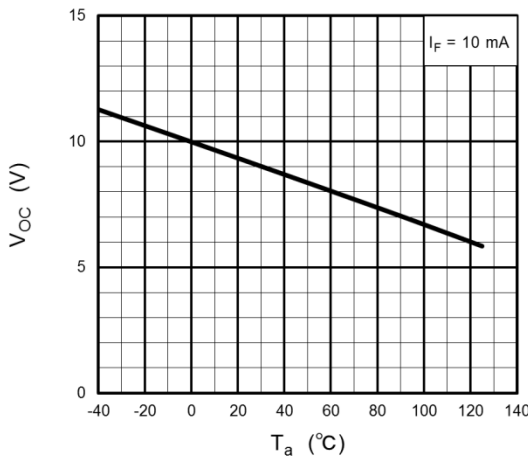


Figure 2.3 TLP3905  $V_{OC}$ - $T_a$  characteristic

2.3  $I_{SC}$ - $I_F$  characteristic

The  $I_{SC}$ - $I_F$  characteristic shows the dependence of short-circuit current ( $I_{SC}$ ) on input forward current ( $I_F$ ). The output short-circuit current ( $I_{SC}$ ) increases as  $I_F$  increases, as shown in Figure 2.4.  $I_{SC}$  charges the gate capacitance of the driven MOSFET. The higher the  $I_{SC}$  value, the shorter the charging time becomes. In other words, increasing  $I_{SC}$  helps reduce the MOSFET turn-on time.

Some photovoltaic-output photocouplers are available with some  $I_{SC}$  ranks. Table 2.2 shows the  $I_{SC}$  ranks for the TLP3905. The TLP3905 with Rank C20 provides an  $I_{SC}$  of minimum 20  $\mu\text{A}$  whereas the TLP3905 without a rank option provides an  $I_{SC}$  of minimum 12  $\mu\text{A}$ . Therefore, Rank C20 makes it possible to control a MOSFET with a high drive capability.

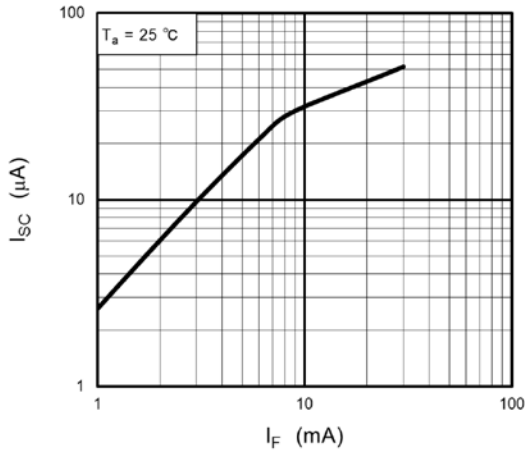


Table 2.2 TLP3905 short-circuit current  $I_{SC}$  rank classification

( $T_a = 25^\circ\text{C}$ )

Rank	$I_{SC}$ Rank Marking	Test Condition	Short-Circuit Current $I_{SC}$ (min)	Unit
C20	C	$I_F = 10 \text{ mA}$	20	$\mu\text{A}$
None	C, Blank	$I_F = 10 \text{ mA}$	12	

Figure 2.4 TLP3905  $I_{SC}$ - $I_F$  characteristic

### 2.4 $I_{SC}$ - $T_a$ characteristic

The  $I_{SC}$ - $T_a$  characteristic shows the dependence of short-circuit current ( $I_{SC}$ ) on the ambient temperature ( $T_a$ ).  $I_{SC}$  decreases as the ambient temperature increases, as shown in Figure 2.5. The  $I_{SC}$ - $T_a$  characteristic is negatively sloped because the light output of an LED decreases as the ambient temperature increases.

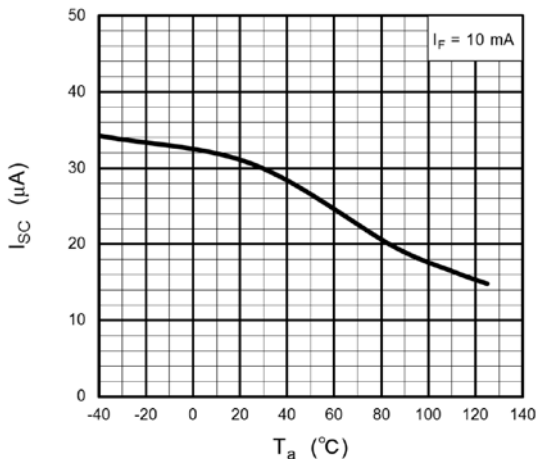


Figure 2.5 TLP3905  $I_{SC}$ - $T_a$  characteristic

### 2.5 $t_{on}$ - $C_L$ and $t_{off}$ - $C_L$ characteristics

The  $t_{on}$ - $C_L$  and  $t_{off}$ - $C_L$  characteristics show the dependence of turn-on and turn-off times ( $t_{on}$  and  $t_{off}$ ) on load capacitance. In the case of a PV+MOSFET relay,  $C_L$  represents the gate capacitance of the driven MOSFET,  $C_g (=Q_g/V_{GE})$ . As the load (i.e., the MOSFET gate capacitance) increases, the time taken to charge and discharge the gate capacitance increases, causing  $t_{on}$  and  $t_{off}$  to increase. Figure 2.6 indicates that, in the case of the TLP3905,  $t_{off}$  can be reduced by using a low-value discharge resistor. However, using a low-value discharge resistor causes the output open voltage ( $V_{OC}$ ) to decrease as indicated by the  $V_{OC}$ - $I_F$  characteristics of Figure 2.1.

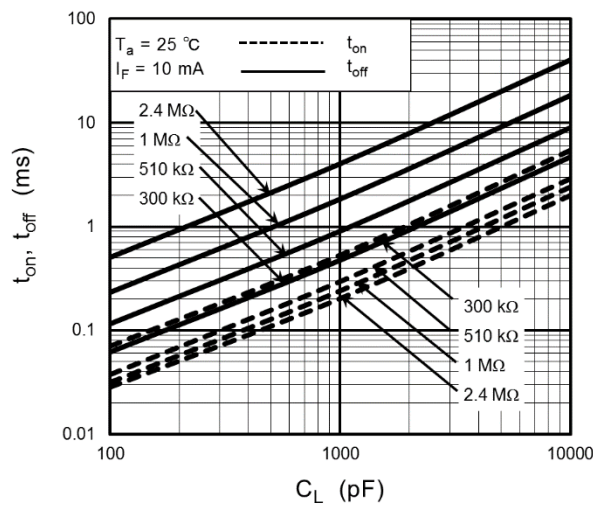


Figure 2.6 TLP3905  $t_{on}$ - $C_L$  and  $t_{off}$ - $C_L$  characteristics

### 3. Considerations for configuring relays with PV+MOSFET combinations

PV+MOSFET relays have many advantages over conventional relays as described thus far. However, careful consideration is necessary because various factors affect their performance as discussed in this section.

PV+MOSFET relays are convenient particularly when you need to:

- Solve the service life and reliability problems of mechanical relays
- Eliminate contact bouncing during turn-off
- Reduce the turn-on and turn-off times
- Provide more intricate control than is achievable with triac- and thyristor-based solid-state relays (SSRs)
- Provide higher off-state output terminal voltage ( $V_{OFF}$ ) and on-state current ( $I_{ON}$ ) than those achievable with photorelays, a type of semiconductor relays. (Toshiba's photorelays are available with a  $V_{OFF}$  of up to 600 V and an  $I_{ON}$  of up to 5 A.)

Figure 3.1 is an example of a semiconductor switch for switching a 24-V/2-A load. The following subsections discuss the considerations for this DC switch.



3.2 Setting the input forward current ( $I_F$ ) and discharge resistor ( $R_{SH}$ ) of the photovoltaic-output photocoupler that satisfy the gate drive condition of the MOSFET

As described in Section 2.2, the  $V_{OC}$  of the photovoltaic-output photocoupler decreases as the ambient temperature increases. The PV+MOSFET relay needs to operate properly at an ambient temperature ( $T_a$ ) of up to 60°C according to the specifications shown in Figure 3.1. In other words, it is necessary to maintain  $V_{OC}$  at a level that satisfies  $V_{GS} = 4.5$  V even at a  $T_a$  of 60°C. From the slope of the  $V_{OC}$ - $T_a$  characteristics shown in Figure 3.3, it is estimated that  $V_{OC}$  should be higher than 5.7 V at a  $T_a$  of 25°C.

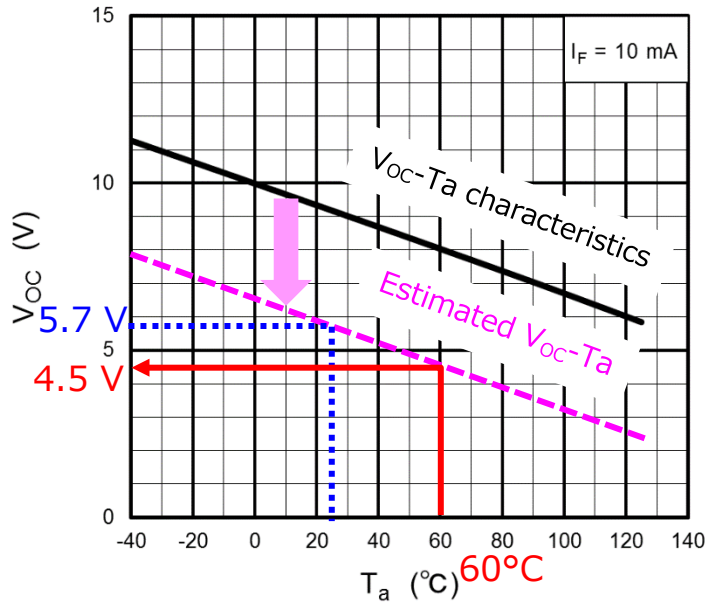


Figure 3.3 TLP3905  $V_{OC}$  - $T_a$  characteristics

Next, look at the  $V_{OC}$ - $I_F$  characteristics of the TLP3905 shown in Figure 3.4.

To turn off a MOSFET, it is necessary to discharge the gate during turn-off. The external resistor ( $R_{SH}$ ) in the circuit of Figure 3.1 serves this purpose. Figure 3.4 shows that its resistance is a parameter that affects the  $V_{OC}$ - $I_F$  characteristics.

Figure 3.4 shows the  $V_{OC}$ - $I_F$  characteristics of the TLP3905 with a typical  $V_{OC}$  of 9 V shown in Figure 3.5. Even if the TLP3905 has a minimum  $V_{OC}$  of 7 V,  $V_{OC}$  will be higher than 5.7 V when  $I_F$  is higher than 10 mA and  $R_{SH}$  is 1 MΩ or higher.

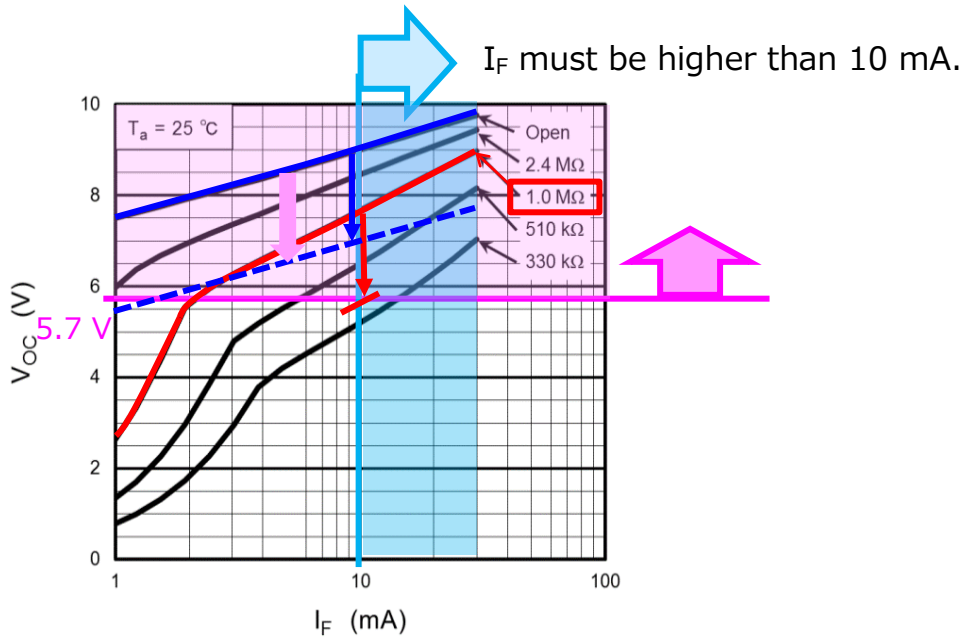


Figure 3.4 TLP3905  $V_{OC}$  - $I_F$  characteristics

( $T_a = 25^\circ\text{C}$ )

Characteristics	Symbol	Note	Test Condition	Min	Typ.	Max	Unit
Open voltage	$V_{OC}$		$I_F = 10\text{ mA}$	7	9	—	V
			$I_F = 10\text{ mA}, T_a = 125\text{ }^\circ\text{C}$	—	5	—	

Figure 3.5 TLP3905  $V_{OC}$  specification

The external discharge resistor ( $R_{SH}$ ) affects both the turn-on and turn-off of the MOSFET. To select an appropriate discharge resistor that satisfies the switching speed requirement, it is necessary to calculate the MOSFET gate capacitance first. When the TPH9R506PL is driven at a  $V_{GS}$  of 4.5 V, its gate capacitance ( $C_g$ ) can be estimated from the  $Q_g$ - $V_{GE}$  characteristics. From the dynamic input/output characteristics of the TPH9R506PL shown in Figure 3.6, the gate charge ( $\Delta Q_g$ ) can be read as 11 nF at a  $V_{DS}$  of 24 V and a  $V_{GS}$  of 4.5 V.

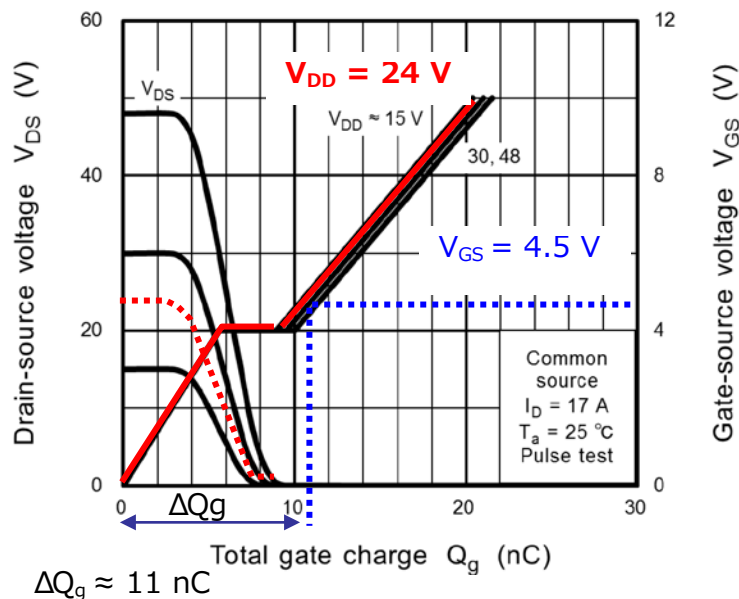


Figure 3.6 TPH9R506PL dynamic input/output characteristics

According to Coulomb's law,  $C_g = Q_g / V_{GE}$ . Hence,  $C_g$  is estimated to be  $11 / 4.5 = 2.4$  nF. The datasheet of the TLP3905 shows the  $t_{on}$ -load capacitance and  $t_{off}$ -load capacitance characteristics (Figure 3.7). In the case of photovoltaic-output photocouplers with a configuration like that of the TLP3905,  $t_{off}$  tends to be predominantly longer than  $t_{on}$ . Figure 3.1 shows that both the  $t_{on}$  and  $t_{off}$  requirements are less than 5 ms. When the load capacitance ( $C_g$ ) is 2.4 nF or greater, the  $t_{on}$  requirement is satisfied regardless of the discharge resistor values shown in Figure 3.7. However, Figure 3.7 indicates that the discharge resistor must be 1 M $\Omega$  or lower to satisfy the  $t_{off}$  requirement.

Now, look at the  $t_{on}$ -load capacitance and  $t_{off}$ -load capacitance characteristics of Figure 3.7. Are they dependent on the  $V_{OC}$  and  $I_{SC}$  parameters of the photovoltaic-output photocoupler?

The turn-off time ( $t_{off}$ ) is determined by the MOSFET gate capacitance ( $C_L$ ) and the discharge resistor value ( $R_{SH}$ ). It is hardly affected by the photovoltaic-output photocoupler. On the other hand, the MOSFET turn-on ( $t_{on}$ ) is the process of charging the gate capacitance ( $C_L$ ) with the output current ( $I_{SC}$ ) from the photovoltaic-output photocoupler. Therefore,  $t_{on}$  increases as  $I_{SC}$  decreases.

Figure 3.7 shows the dynamic input/output characteristics of the TLP3905 with a standard rank ( $I_{SC} \approx 30$   $\mu$ A) described in Sections 2.3 and 2.4. Assuming that  $I_{SC}$  is at the minimum,  $I_{SC}$  can be estimated as follows at an  $I_F$  of 10 mA:

In the case of the C20  $I_{SC}$  rank, when  $T_a = 25^\circ\text{C}$ ,  $I_{SC}(\text{typ}) = 30$   $\mu$ A  $\rightarrow$   $I_{SC}(\text{min}) = 20$   $\mu$ A

When  $T_a$  increases from  $25^\circ\text{C}$  to  $60^\circ\text{C}$ ,  $I_{SC}$  decreases by 20%. That is:  $I_{SC}(\text{min}) = 20$   $\mu$ A at  $T_a = 25^\circ\text{C} \rightarrow 16$   $\mu$ A at  $T_a = 60^\circ\text{C}$

Taking this into consideration, it is necessary to assume that the  $t_{on}$  values shown in Figure 3.7 can differ by roughly 1.9 times at the typical and minimum  $I_{SC}$  (30  $\mu$ A / 16  $\mu$ A). However, in the case of our DC switch,  $t_{on}$  will not exceed  $t_{off}$  even at the minimum  $I_{SC}$ .

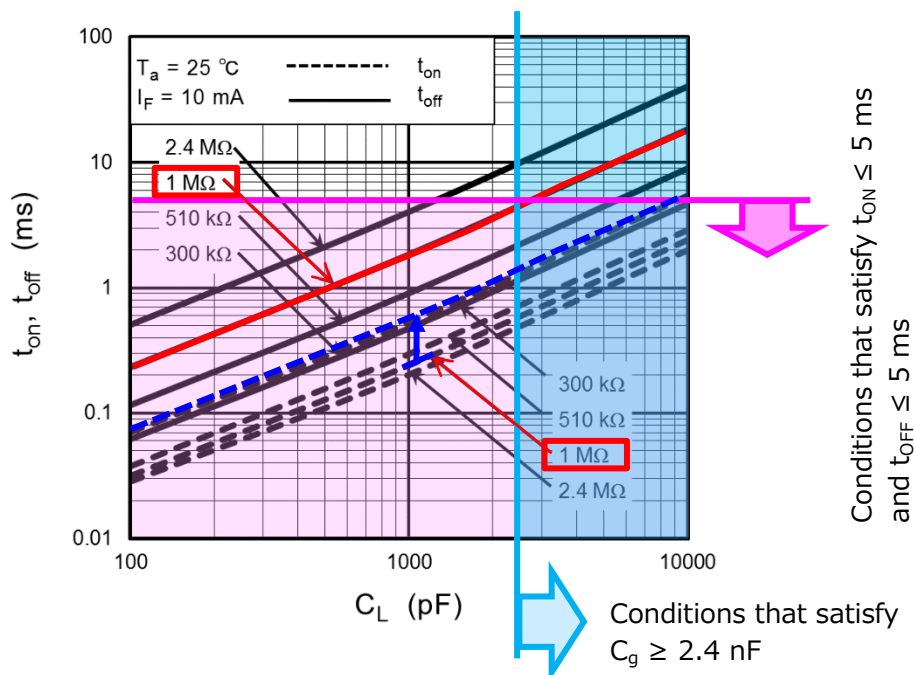


Figure 3.7 TLP3905  $t_{on}$ ,  $t_{off}$  -load capacitance ( $C_L$ ) characteristics



### 3.3 Input forward current ( $I_F$ ) of the photovoltaic-output photocoupler and selection of $R_{IN}$ based on $I_F$

In Section 3.2, the conditions that satisfy  $I_F > 10 \text{ mA}$  were estimated. Now, remember that the light output of the input LED decreases over time. The degradation of the LED depends on its input current and the number of hours of operation. A reduction in the output short-circuit current ( $I_{SC}$ ) is highly dependent on a reduction in the LED's light output. Figure 3.8 shows the degradation of the light output of the LED incorporated in the TLP3905. Suppose that the expected service life is 10 years (roughly 88,000 hours). Figure 3.8 shows that the light output decreases to roughly 85% after 10 years of operation. Allowing for a margin, assume that the light output will decrease to 80% of the initial output after 10 years of use (i.e., a 20% decrease).

Taking the degradation in the light output into consideration,  $I_F$  should be set to  $10 \text{ mA} / 0.8 = 12.5 \text{ mA}$ .

Let the low-level output voltage of the logic IC that drives the input LED be  $V_{OL}$ . Then,  $I_{F(typ.)}$  is expressed as:

$$I_{F(typ.)} = \frac{V_{CC} - V_{F(typ.)} - V_{OL}}{R_{IN(typ.)}}$$

The datasheet of the TLP3905 shows:

$$V_{F(typ.)} = 1.65 \text{ V} \quad (I_F = 10 \text{ mA})$$

Hence:

$$R_{IN} = \frac{5\text{V} - 1.65\text{V} - 0.4\text{V}}{12.5\text{mA}}$$

$$= 236 \Omega$$

Therefore, a resistor with  $240 \Omega \pm 5\%$  should be selected as  $R_{IN}$ .

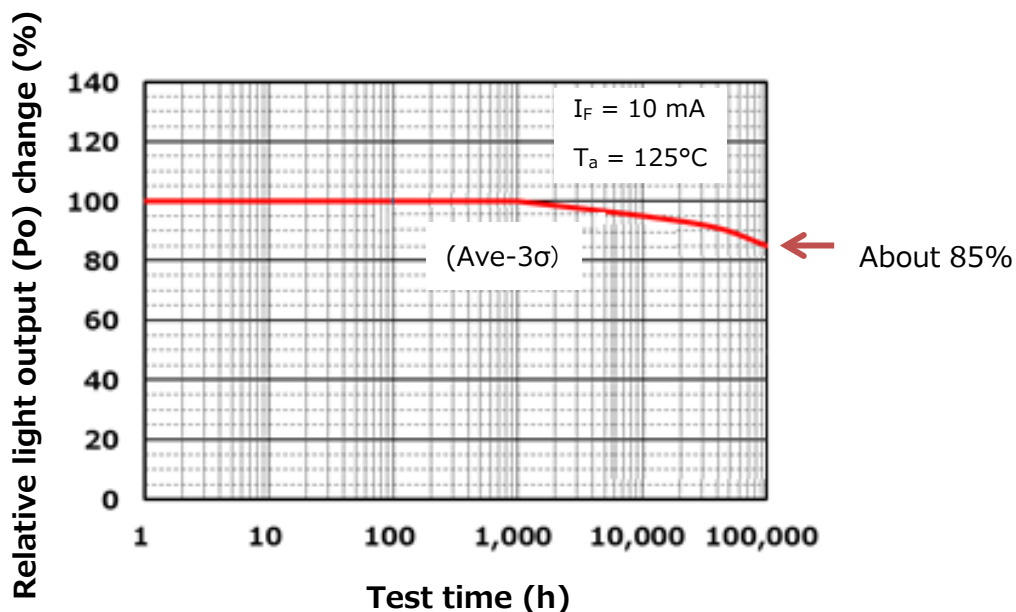


Figure 3.8 Example of LED light output degradation curve

(The above graph shows a typical LED light output degradation curve. When designing a circuit incorporating photocouplers such as the TLP3905, consult the reliability data of each photocoupler.)

In this example,  $V_{OC}$  is greater than  $V_{GS} = 4.5\text{ V}$  even at a  $T_a$  of  $60^\circ\text{C}$ . If the relationship  $V_{OC} > V_{GS} (V_{th})$  cannot be satisfied, sufficient gate voltage can be obtained by connecting multiple photovoltaic-output photocouplers in series.

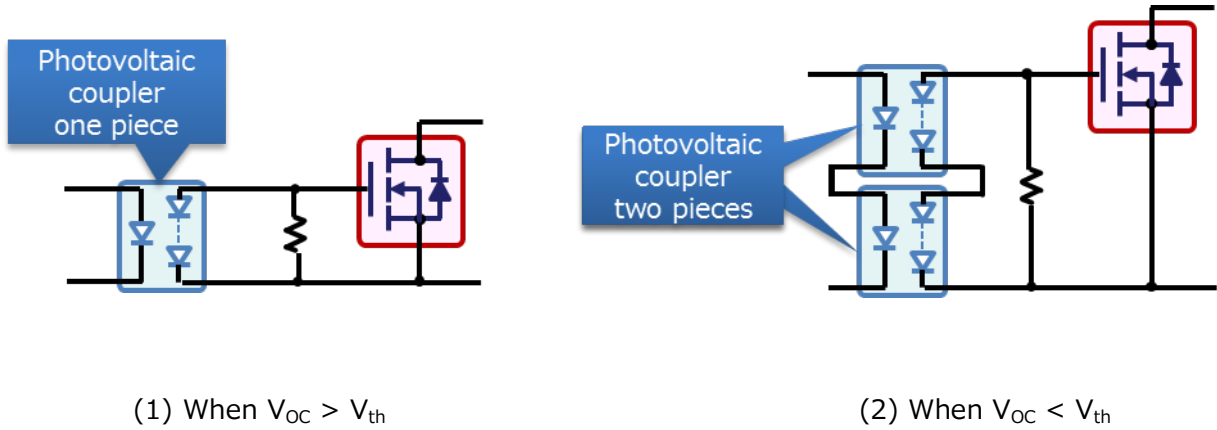


Figure 3.9 Study for the photovoltaic-output photocoupler configuration based on the MOSFET  $V_{th}$  requirement

### 4. Terms

#### (General terms)

Term	Symbol	Description
Absolute Maximum Rating		Maximum value that must not be exceeded even for an instant during operation
Isolation Voltage	$BV_S$	Isolating voltage between input and output under the specified conditions
Capacitance (Input to Output), Total Capacitance (Input to Output)	$C_S$	Electrostatic capacitance between the input and output pins
Capacitance (Input), Input Capacitance	$C_T$ $C_t$	Electrostatic capacitance between the anode and cathode pins of the LED
Forward Current, Input Forward Current	$I_F$	Rated current that can flow continuously in the forward direction of the LED
Pulse Forward Current, Input Forward Current (Pulsed)	$I_{FP}$	Rated current that can flow momentarily in the forward direction of the LED
Peak Transient Forward Current	$I_{FPT}$	Rated current that can flow momentarily in the forward direction of the LED
Reverse Voltage, Input Reverse Voltage	$V_R$	Rated reverse voltage that can be applied across the LED's cathode and anode
Reverse Current, Input Reverse Current	$I_R$	Leakage current flowing in the reverse direction of the LED (from cathode to anode)
Forward Voltage, Input Forward Voltage	$V_F$	Voltage drop across the anode and cathode pins of the LED under the specified forward-current condition
LED Power Dissipation, Input Power Dissipation	$P_D$	Rated power that can be dissipated in the LED
Total Power Dissipation	$P_T$	Total rated power that can be dissipated in both the input and output devices
Isolation Resistance	$R_S$	Resistance between the input and output pins at the specified voltage
Junction Temperature	$T_j$	Permissible temperature of the junction of the photodetector or LED
Operating Temperature	$T_{opr}$	Ambient temperature range in which the device can operate without loss of functionality
Lead Soldering Temperature	$T_{sol}$	Rated temperature at which the device pins can be soldered without loss of functionality
Storage Temperature	$T_{stg}$	Ambient temperature range in which the device can be stored without operation
Creepage Distance		Shortest distance along the surface of insulation between the path of two conductive parts (input and output)
Clearance(Clearance Distance)		Shortest distance through air between the path of two conductive parts (input and output)
Internal Isolation Thickness, Insulation Thickness		Distance through insulation. Shortest thickness through internal insulation between the path of two conductive parts (input and output)

### (Photovoltaic output)

Term	Symbol	Description
Forward Current, Output Forward Current	$I_{FD}$	Rated forward current that can be applied between anode and cathode of the output diode array
Reverse Voltage, Output Reverse Voltage	$V_{RD}$	Rated reverse voltage that can be applied across anode and cathode of the output diode array
Forward Voltage, Output Forward Voltage	$V_{FD}$	Forward voltage across the output's anode and cathode
Reverse Current, Output Reverse Current	$I_{RD}$	Reverse leakage current between the output's anode and cathode
Open Voltage	$V_{OC}$	Output photovoltaic voltage generated by the specified input current, $I_F$
Short-Circuit Current	$I_{SC}$	Output photo-current generated by the specified input current, $I_F$

### (Photorelay (MOSFET output))

Term	Symbol	Description
Trigger LED Current	(Contact a) $I_{FT}$	Minimum input current, $I_F$ , necessary to turn on the output MOSFET (*1)
	(Contact b) $I_{FC}$	Minimum input current, $I_F$ , necessary to turn off the output MOSFET (*1)
Return LED Current	(Contact a) $I_{FC}$	Maximum input current, $I_F$ , necessary to return the output MOSFET to the OFF state
	(Contact b) $I_{FT}$	Maximum input current, $I_F$ , necessary to return the output MOSFET to the ON state
OFF-State Output Terminal Voltage	$V_{OFF}$	Rated voltage that can be applied across the MOSFET's output pins in the OFF state
ON-State Current	$I_{ON}$	Rated current that can flow between the MOSFET's output pins in the ON state
ON-State Resistance	$R_{ON}$	Resistance between the MOSFET's output pins under the specified ON-state conditions
OFF-State Current	$I_{OFF}$	Leakage current flowing between the MOSFET's output pins in the OFF state
Load Current Limiting	$I_{LIM}$	Output current range in which the current limiting function is tripped
Output Capacitance	$C_{OFF}$	Capacitance between the MOSFET's output pins (between the two drains)
Turn-ON Time	(Contact a) $t_{ON}$	Time taken for the output waveform to change from 100% to 10% after the LED current is turned on under the specified conditions
	(Contact b) $t_{ON}$	Time taken for the output waveform to change from 100% to 10% after the LED current is turned off under the specified conditions
Turn-OFF Time	(Contact a) $t_{OFF}$	Time taken for the output waveform to change from 0% to 90% after the LED current is turned off under the specified conditions
	(Contact b) $t_{OFF}$	Time taken for the output waveform to change from 0% to 90% after the LED current is turned on under the specified conditions

(\*1)  $I_F$  greater than the maximum  $I_{FT}$  ( $I_{FC}$ ) is required to ensure that the photorelay transitions from the OFF (ON) state to the ON (OFF) state.

### Revision history

Version	Date	Page	Description
Rev. 1.0	2019-04-25	-	First edition

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