## High-Voltage Intelligent Power Devices Application Note(SSOP30)

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## 1. Products discussed herein

### 1.1. Product offerings

Table 1.1 High-voltage intelligent power devices

| Part Number | Ratings | Features |  |  |  |  |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 6-Input | 3-Phase <br> Distribution PWM Circuit | Level-Shifter \& Driver | over-current Protection | Thermal Shutdown | Under voltage Protection |  |
| TPD4204F | $\begin{gathered} 600 \mathrm{~V} / \\ 2.5 \mathrm{~A} \end{gathered}$ | Y | - | Y | Y | Y | Y | $\begin{gathered} 180^{\circ} \\ \text { (Note) } \end{gathered}$ |
| TPD4206F | $\begin{gathered} 500 \mathrm{~V} / \\ 2.5 \mathrm{~A} \end{gathered}$ | Y | - | Y | Y | Y | Y | $\begin{gathered} 180^{\circ} \\ \text { (Note) } \end{gathered}$ |
| TPD4207F | $\begin{gathered} 600 \mathrm{~V} / \\ 5 \mathrm{~A} \end{gathered}$ | Y | - | Y | Y | Y | Y | $\begin{gathered} 180^{\circ} \\ (\text { Note }) \end{gathered}$ |

Note: In combination with a microcontroller unit (MCU) or a motor controller IC

HVIPDs for sine-wave (180-degree) type
The HVIPDs can be used in combination with Toshiba's motor controller IC or MCU to drive a motor with sine-wave (180-degree) type so as to reduce its acoustic noise and vibration.


Figure 1.1 Block diagram for an HVIPD for sine-wave (180-degree) type

Table 1.2.1 Controller IC list sine-wave drive type (Example of products)

| Part Number | Package | Vcc / Io | Position Sensing | Features |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Lead <br> Angle <br> Contro | Built-in Oscillator | Overcurrent Protection | Gate <br> Block Protection | Position Signal Abnormality Protection | $V_{c c}$ <br> Under <br> voltage <br> Protection |
| TB6551FAG | SSOP24 | 12V/2mA | Hall effect IC | External setting | - | Y | Y | Y | Y |
| TB6556FG | SSOP30 | 12V/2mA |  | Current <br> Feedback | - | Y | Y | Y | Y |
| TB6584FNG/AFNG <br> (Note 1) | SSOP30 | 18V/2mA | Hall element or Hall effect IC |  | Y | Y | Y | Y | Y |
| TB6634FNG | SSOP30 | 18V/2mA |  |  | Y | Y | Y | Y | Y |
| TB6631FNG | SSOP30 | 18V/2mA |  | RPM <br> Feedback <br> (Note 2) | Y | Y | Y | Y | Y |
| TC78B041FNG | SSOP30 | 18V/2mA |  | Intelligent <br> Phase <br> Control <br> (Note 3) | Y | Y | Y | Y | Y |
| TC78B042FTG | QFN32 | 18V/2mA |  |  | Y | Y | Y | Y | Y |

Note 1: Specifications such as modulation generation method and automatic advance angle mode differ.
Refer to the data sheet of each product for details.
Note 2: Internal auto lead angle control based on the frequency of the FG signal.
Note 3: Toshiba's original automatic phase adjustment function.
Table 1.2.2 Microcomputer list sine-wave drive type (Example of products)

| Part Number | Package | ROM Size (Bytes) | RAM Size <br> (Bytes) | Max. <br> Operating <br> Frequency $(\mathrm{MHz})$ | Operating Voltage (V) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min | Max |
| TMPM375FSDMG | SSOP30 | 64 K | 4 K | 40(Note 1) | 4.5 | 5.5 |
| TMPM372FWUG | LQFP64 | 128 K | 6 K | $\begin{aligned} & 80(\text { Note } 2) \\ & 32(\text { Note } 1) \end{aligned}$ | 4.5 | 5.5 |
| TMPM373FWDUG | LQFP48 |  |  |  |  |  |
| TMPM374FWUG | LQFP44 |  |  |  |  |  |
| TMPM370FYDFG | QFP100 | 256 K | 10 K | 80(Note 2) | 4.5 | 5.5 |
| TMPM370FYFG | LQFP100 |  |  |  |  |  |
| TMPM376FDDFG | QFP100 | 512 K | 32 K | 80(Note 2) | 4.5 | 5.5 |
| TMPM376FDFG | LQFP100 |  |  |  |  |  |

Note 1: Ambient temperature $-40^{\circ} \mathrm{C} \sim 105^{\circ} \mathrm{C}$
Note 2: Ambient temperature $-40^{\circ} \mathrm{C} \sim 85^{\circ} \mathrm{C}$

## 2. Outline dimensions and marking of the SSOP30 package

The SSOP30 package simplifies board trace routing because it has high-voltage and control
pins on opposite sides. In addition, the SSOP30 package is thin and small.

### 2.1. Package outline dimensions

P-SSOP30-1120-1.00-001
Unit: mm


Figure 2.1 Outline dimensions of the SSOP30 package

### 2.2. Marking



When Lot code is 『 $930 』$, it expressed that having been manufactured at the 30th week in 2019.

Figure 2.2 Part marking on the SSOP30 package
2.3. PCB land pattern dimensions (Reference)


Figure 2.3 Land pattern of the SSOP30(Reference)

### 2.4. Soldering

Recommended soldering methods
Table 2.4 Adaptation table

| Reflow soldering | Flow soldering | Soldering iron |
| :---: | :---: | :---: |
| 3 times maximum | Not supported | Only once |

1) Reflow

Peak temperature : Maximum $260^{\circ} \mathrm{C}$ / a moment
Internal device temperature / period : $230^{\circ} \mathrm{C}$ or more / 30 to 50 seconds
Pre-heat temperature / period : 180 to $190^{\circ} \mathrm{C} / 60$ to 120 seconds
Note: Maximum mounting temperature is based on package surface temperature.
Figure 2.4 shows the temperature profile.
This profile represents the maximum device temperature at which device performance can be guaranteed. The preheat temperature and heating temperature will be governed by factors such as the type of solder paste used, but must be within the range shown in Figure 2.4.

The package is carefully wrapped to be protected against humidity. After unwrapping, the package should be maintained at $30^{\circ} \mathrm{C}$ and $60 \% \mathrm{RH}$ until the final reflow stage, and mounting should be completed within 168 hours.


Figure 2.4 Example of a reflow soldering profile
2) Flow

This package is not suitable for solder flow mounting.
3) Soldering iron

Heating method : Via lead tip of soldering iron
Heating condition : $400^{\circ} \mathrm{C}$ (at tip) for no more than 3 sec
Repetitions: No repetitions (once only per terminal)

- Note:

Check solder bonding strength via in house testing at the substrate mounting stage.

### 2.5. Attaching a heatsink

A heatsink may be required, depending on the ambient temperature or the heating of the HVIPD or its neighboring devices. Attach a heatsink as described below if necessary.

- Heatsink attachment example

1) Example of using an insulating sheet


Table 2.5.1 Example of parts used

| Screw | M3 |
| :---: | :--- |
| Insulating <br> sheet | Soft <br> material <br> $t=0.5 \mathrm{~mm}$ |
| Height <br> spacer | $\mathrm{t}=2.5 \mathrm{~mm}$ <br> Holes:3.2Ф |

Figure 2.5.1 Heatsink attachment example (using an insulating sheet)
2) Example of using resin or gelatinous insulating material


Figure 2.5.2 Heatsink attachment example (using resin or gelatinous insulating material)
3) Example of other heatsink attachment method


Soldering
Figure 2.5.3 Soldering


Pushpin
Figure 2.5.4 Pushpin


Figure 2.5.5 Adhesion attachment

The result of having measured the case temperature in the substrate for evaluation which attached the radiator plate with soldering is shown in reference.
Evaluation conditions: $\mathrm{V}_{\mathrm{BB}}=280 \mathrm{~V}, \mathrm{~V}_{\mathrm{CC}}=15 \mathrm{~V}$, motor number of rotations =regularity (1500rpm),

$$
\mathrm{fc}=16.5 \mathrm{kHz}, \mathrm{Ta}=25^{\circ} \mathrm{C}
$$

In combination with substrate for our company evaluation (TPD4204F+TB6551FAG), Heatsink (three types), Variable of the load of a fan motor is carried out, and case temperature is measured.


Figure 2.5.6 The substrate for evaluation, and a temperature survey position
Table 2.5.2 Example of a model name of heatsink

| TYPE-A | TYPE-B | TYPE-C |
| :---: | :---: | :---: |
|  |  |  |
| Sankyo Thermo Tech Type:20FSH036-L36-WFL-B With a terminal <br> Length:36 $\times$ Width:36 $\times$ <br> Height:20mm <br> Surface area: $115 \mathrm{~cm}^{2}$ | Sankyo Thermo Tech Type:20FSH036-L64-WFL-B <br> With a terminal <br> Length:36 $\times$ Width:64 $\times$ <br> Height:20mm <br> Surface area:202cm² | Sankyo Thermo Tech Type:16FSH064-L36-WFL-B <br> With a terminal <br> Length:36 $\times$ Width:64: $\times$ <br> Height:16mm <br> Surface area: $163 \mathrm{~cm}^{2}$ |



Figure 2.5.7 Input electric power $(\mathrm{Pi})-\Delta \mathrm{Tc}$ and power loss- $\Delta \mathrm{Tc}$ in various heatsink

- Mounting to substrate

Where the SSOP30 package is sandwiched between the heat sink and the substrate, it the static load should be no greater than 10 N . The load should be spread uniformly across the device, and screw mountings should not result in substrate


Figure 2.5.8 Bent PCB bending as shown in right Figure, as the resulting distortion could cause device damage or failure. Consider using spacers or equivalent to attach the heat sink so as to prevent substrate bending.

## -Flatness

The surface beneath the heat sink to which the device is attached must be suitably smooth and flat. The heat sink should likewise show no signs of warping or undulation and should be free of foreign matter such as burrs and scraps from pressing and cutting processes. In the worst case scenario this could lea d to device failure. And heat fins fixed to the top of the package can cause device failure due to heat stress. Hard components (such as the heat sink) should be mounted onto the package together with a buffer layer (typically soft insulating sheet or conductive gel). Silicon grease should be avoided.

## 3. Pin description

### 3.1. Pin assignment

Table 3.1 Pin description

| Pin No. | Symbol |  |
| :---: | :---: | :--- |
| 1 | NC | No-connect pin, which is not connected to the internal chip |
| 2 | NC | No-connect pin, which is not connected to the internal chip |
| 3 | NC | No-connect pin, which is not connected to the internal chip |
| 4 | DIAG | Open-drain diagnostic output. Connect a pull-up resistor to the DIAG pin. The DIAG <br> pin is driven Low in the event of a fault (an overcurrent, overtemperature, or under <br> voltage condition). |
| 5 | V $_{\text {CC }}$ | Control power supply pin (15V typical) |


| 6 | $V_{\text {REG }}$ | 7V regulator output pin |
| :---: | :---: | :---: |
| 7 | SD | External protection input (Active-Low, no hysteresis) |
| 8 | GND | Ground pin |
| 9 | RS | Overcurrent detection pin |
| 10 | LW | Control pin for the low-side Phase-W MOSFET. The MOSFET turns off when LW $\leq$ 1.5 V and turns on when $\mathrm{LW} \geq 2.5 \mathrm{~V}$. |
| 11 | LV | Control pin for the low-side Phase-V MOSFET. The MOSFET turns off when LV $\leq 1.5$ V and turns on when $\mathrm{LV} \geq 2.5 \mathrm{~V}$. |
| 12 | LU | Control pin for the low-side Phase-U MOSFET. The MOSFET turns off when LU $\leq 1.5$ V and turns on when $\mathrm{LU} \geq 2.5 \mathrm{~V}$. |
| 13 | HW | Control pin for the high-side Phase-W MOSFET. The MOSFET turns off when HW $\leq$ 1.5 V and turns on when $\mathrm{HW} \geq 2.5 \mathrm{~V}$. |
| 14 | HV | Control pin for the high-side Phase-V MOSFET. The MOSFET turns off when HV $\leq$ 1.5 V and turns on when $\mathrm{HV} \geq 2.5 \mathrm{~V}$. |
| 15 | HU | Control pin for the high-side Phase-U MOSFET. The MOSFET turns off when HU $\leq$ 1.5 V and turns on when $\mathrm{HU} \geq 2.5 \mathrm{~V}$. |
| 16 | GND | Ground pin |
| 17 | NC | No-connect pin, which is not connected to the internal chip |
| 18 | NC | No-connect pin, which is not connected to the internal chip |
| 19 | NC | No-connect pin, which is not connected to the internal chip |
| 20 | IS3 | Source pin for the Phase-W MOSFET |
| 21 | W | Phase-W output pin |
| 22 | BSW | Phase-W bootstrap capacitor connection pin |
| 23 | $V_{B B}$ | High-voltage power supply pin |
| 24 | $\mathrm{V}_{\text {BB }}$ | High-voltage power supply pin |
| 25 | BSV | Phase-V bootstrap capacitor connection pin |
| 26 | V | Phase-V output pin |
| 27 | IS2 | Source pin for the Phase-V MOSFET |
| 28 | IS1 | Source pin for the Phase-U MOSFET |
| 29 | BSU | Phase-U bootstrap capacitor connection pin |
| 30 | U | Phase-U output pin |

* The NC pins are no-connect pins that are not connected to the internal chip.

Even if the NC pins are left open, they do not affect the electrical characteristics of the device. However, we recommend soldering them onto a PCB.

## 4. Functional descriptions and usage considerations

### 4.1. Protection features

## Under voltage protection

The HVIPD incorporates an under voltage protection circuit, which prevents internal MOSFETs from operating in an unsaturated region when the $\mathrm{V}_{\mathrm{CC}}$ and $\mathrm{V}_{\mathrm{BS}}$ voltages drop. When $\mathrm{V}_{\mathrm{CC}}$ drops to $\mathrm{V}_{\mathrm{CC}} U V D$ ( $=11 \mathrm{~V}$ typical), all the MOSFET outputs shut down regardless of the input states. Under voltage protection has a hysteresis of 0.5 V . When $\mathrm{V}_{\mathrm{cc}}$ rises back to $\mathrm{V}_{\mathrm{CC}} \mathrm{UVR}$ ( $=11.5 \mathrm{~V}$ typical), the MOSFETs return to normal operation and turn on according to the input states. When $\mathrm{V}_{\mathrm{cc}}$ under voltage protection is tripped, the DIAG output toggles its state. However, the DIAG output might remain unchanged if $V_{C C}$ is lower than 7 V . (All the MOSFET outputs shut down when $\mathrm{V}_{\mathrm{cc}}$ drops below 11V, even if the DIAG output does not toggle.) When $\mathrm{V}_{\mathrm{BS}}$ drops to
$\mathrm{V}_{B S} U V D$ ( $=10 \mathrm{~V}$ typical), all the high-side MOSFET outputs shut down. When $\mathrm{V}_{\mathrm{BS}}$ rises back to $V_{B S} U V R$ ( $=10.5 \mathrm{~V}$ typical), 0.5 V higher than $V_{B S} U V D$, the high-side MOSFETs return to normal operation and operate according to the control signals. $\mathrm{V}_{\mathrm{BS}}$ under voltage protection does not cause the DIAG output to toggle.


Figure 4.1.1 $\mathrm{V}_{\mathrm{cc}}$ Under voltage protection


Figure 4.1.2 $\mathrm{V}_{\mathrm{BS}}$ Under voltage protection

## Overcurrent protection

The HVIPD incorporates a current limiter, which protects itself from excessive current at motor startup or when the rotor is locked. The current limiter senses the voltage across the currentsensing resistor connected to the RS pin. When this voltage exceeds $\mathrm{V}_{\mathrm{R}}$ ( $=0.5 \mathrm{~V}$ typical), the MOSFET outputs temporarily shut down after a delay of $3 \mu \mathrm{~s}$ (typical) to prevent a further
increase in current. Setting the control signals to all-Lows releases the HVIPD from currentlimiting mode.

Selecting a current-limiting resistor:
$\mathrm{I}_{\mathrm{O}}=\mathrm{V}_{\mathrm{R}} \div \mathrm{R}_{1}$
$\mathrm{V}_{\mathrm{R}}$ : Current-limiting voltage, I : Current limit, $\mathrm{R}_{1}$ : Current-limiting resistor

Table 4.1 Current-limiting voltage (from the Electrical Characteristics table) Unit: V

| Characteristics | Symbol | Min | Typ. | Max |
| :--- | :---: | :---: | :---: | :---: |
| Current-limiting <br> voltage | $\mathrm{V}_{\mathrm{R}}$ | 0.46 | 0.5 | 0.54 |

Setting the current-limiting delay time
The HVIPD incorporates a filter shown in Figure 4.1 .3 to prevent the current limiter from malfunctioning because of the noise at the current-limiting resistor. The delay time from when the current limiter senses a current exceeding the current limit to when the MOSFETS outputs shut down is determined by the sum of the filtering time (dead time) of the filter and the delay time of the control circuit:
Current-limiting delay time $\left(D_{t}\right)=$ filtering time (dead time) + control circuit delay If the current-limiting resistor has large noise, the dead time of the internal filter may be insufficient. In that case, an external filter should be added as shown below. Note that an external filter increases the current-limiting delay time (i.e., the time required for the MOSFET outputs to shut down).
Table 4.2 Current-limiting delay time (from the Electrical Characteristics table)

| Unit: $\boldsymbol{\mu s}$ |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Characteristics | Symbol | Min | Typ. | Max |  |
| Current-limiting <br> delay time | $\mathrm{D}_{\mathrm{t}}$ | 1.5 | 3 | 5 |  |



Figure 4.1.3 Internal circuit of the RS pin


Figure 4.1.4 Overcurrent protection operation

## Thermal shutdown

The HVIPD incorporates a thermal shutdown circuit to protect itself from excessive temperature. When an external factor or internally generated heat causes the chip temperature to rise to the thermal shutdown temperature (TSD), all the MOSFET outputs shut down regardless of the input states. Thermal shutdown has a hysteresis ( $\triangle T S D$ ) of $50^{\circ} \mathrm{C}$ typical. When the chip temperature drops below (TSD - $\Delta$ TSD), the MOSFETs return to normal operation and turn on according to the input states.
The HVIPD senses its chip temperature at one position. Suppose that MOSFETs are heat sources. The time taken to shut down the MOSFETs differs, depending on the distance between a heat source and the temperature sensor. Therefore, the chip temperature may be higher than the thermal shutdown temperature (TSD) when the thermal shutdown circuit is tripped.


Figure 4.1.5 Thermal shutdown operation

## SD function

An overcurrent condition may be detected by an external circuit. Setting the SD pin Low causes all the MOSFET outputs to shut down after a delay of $2 \mu \mathrm{~s}$ (typical). Setting the control signals to all-Lows releases the MOSFETs from shutdown mode.

## 4.2. $\mathrm{V}_{\text {REG }}$ power supply

A regulated supply voltage from the $\mathrm{V}_{\text {REG }}$ pin is generated from the $\mathrm{V}_{\mathrm{CC}}$ power supply. $\mathrm{V}_{\text {REG }}$ can be used as a power supply not only for the internal circuit but also for an external control IC or other peripheral ICs.
Add an external capacitor to the $\mathrm{V}_{\text {REG }}$ pin to prevent oscillation. A capacitor with a value of 0.1
$\mu \mathrm{F}$ to $1 \mu \mathrm{~F}$ is recommended.
As $I_{\text {REG }}$ increases, $\mathrm{V}_{\text {REG }}$ becomes more susceptible to oscillation. Adjust the value of the capacitor if $\bigvee_{\text {REG }}$ oscillates under actual usage conditions. Table 4.2 shows the $\bigvee_{\text {REG }}$ output voltage.

Table 4.2 Regulator voltage (at $\mathrm{V}_{\mathrm{CC}}=15 \mathrm{~V}, \mathrm{I}_{\mathrm{REG}}=30 \mathrm{~mA}$ ) Unit: V

| Min | Typ. | Max |
| :---: | :---: | :---: |
| 6.5 | 7 | 7.5 |

### 4.3. Power supply sequencing

We do not recommend the following power sequences:
At power-up: Powering up $\mathrm{V}_{\mathrm{CC}}$ after $\mathrm{V}_{\mathrm{BB}}$ and control signals
At power-down: Powering down $\mathrm{V}_{\mathrm{CC}}$ before $\mathrm{V}_{\mathrm{BB}}$ and control signals

Table 4.3.1 At power-up

| $A t$ power-up |  |  | $\bigcirc / \times$ |
| :---: | :---: | :---: | :---: |
| 1 | 2 | (3) |  |
| $\mathrm{V}_{\mathrm{CC}}$ | $\mathrm{V}_{\mathrm{BB}}$ | Control signals | $\bigcirc$ |
| $\mathrm{V}_{\mathrm{CC}}$ | Control signals | $\mathrm{V}_{\mathrm{BB}}$ | $\bigcirc$ |
| $\mathrm{V}_{\mathrm{BB}}$ | $\mathrm{V}_{\mathrm{CC}}$ | Control signals | $\bigcirc$ |
| $\mathrm{V}_{\mathrm{BB}}$ | Control signals | $\mathrm{V}_{\mathrm{CC}}$ | $\times$ |
| Control signals | $\mathrm{V}_{\mathrm{CC}}$ | $\mathrm{V}_{\mathrm{BB}}$ | $\bigcirc$ |
| Control signals | $\mathrm{V}_{\mathrm{BB}}$ | $\mathrm{V}_{\mathrm{CC}}$ | $\times$ |

Table 4.3.1 At power-down

| At power-down |  |  | $\bigcirc / \times$ |
| :---: | :---: | :---: | :---: |
| (1) | (2) | (3) |  |
| $\mathrm{V}_{\text {cc }}$ | $\mathrm{V}_{\text {BB }}$ | Control signals | $\times$ |
| $\mathrm{V}_{\text {cc }}$ | Control signals | $\mathrm{V}_{\text {BB }}$ | $\times$ |
| $\mathrm{V}_{\text {BB }}$ | $\mathrm{V}_{\mathrm{cc}}$ | Control signals | $\bigcirc$ |
| $\mathrm{V}_{\text {BB }}$ | Control signals | $\mathrm{V}_{\text {cC }}$ | $\bigcirc$ |
| Control signals | $\mathrm{V}_{\text {cc }}$ | $\mathrm{V}_{\text {BB }}$ | $\bigcirc$ |
| Control signals | $\mathrm{V}_{\text {BB }}$ | $\mathrm{V}_{\text {cc }}$ | $\bigcirc$ |

O: Recommended, $\times$ : Unrecommended
Note that even when $V_{C C}$ and $V_{B B}$ are powered down, the device might be permanently damaged if the $V_{B B}$ line is disconnected by a relay or other means while the motor is running because this blocks a current recirculation path to $\mathrm{V}_{\mathrm{BB}}$.

### 4.4. Calculating power losses

This section shows how to calculate power losses that occur when the output current is sinusoidal.
$P=P_{\text {on }}+P_{t}+P_{i B B}+P_{i c c}$
(1) Conduction loss: $P_{o n}$
$P_{\text {on }}=P_{H}+P_{L}+P_{D}(W)$
-High-side MOSFET conduction loss: $\mathrm{P}_{\mathrm{H}}=\mathrm{I}^{2} \times \mathrm{RonH}_{\mathrm{on}} \times(1 / 8+\mathrm{D} / 3 \pi \times \cos \theta) \times 3$
-Low-side MOSFET conduction loss: $\mathrm{P}_{\mathrm{L}}=\mathrm{I}^{2} \times \mathrm{RonL} \times(1 / 8+\mathrm{D} / 3 \pi \times \cos \theta) \times 3$
$\bullet$ Flywheel diode conduction loss: $P_{D}=I \times V_{F} \times(1 / 8-D / 3 \Pi \times \cos \theta) \times 6$
$\mathrm{I}_{\mathrm{p}}$ : Peak motor winding current (A)
$\mathrm{R}_{\text {onн }} / \mathrm{R}_{\text {onL }}$ : On-resistance of the output MOSFET ( $\Omega$ )
$V_{F}$ : Forward voltage drop of the FRD (V)
D: PWM duty cycle (on-duty cycle of the high-side MOSFETs)
$\theta$ : Power factor
(2) MOSFET switching loss: $\mathrm{Pt}_{\mathrm{t}}$
$P_{t}=\left(W_{\text {ton }}+W_{\text {toff }}\right) \times \mathrm{f}_{\mathrm{c}} / \pi \times 6(\mathrm{~W})$

- $W_{\text {ton }}$ : Turn-on loss ( $\mu \mathrm{J}$ per pulse)
- $W_{\text {toff: }}$ Turn-off loss ( $\mu \mathrm{J}$ per pulse)
$\bullet f \mathrm{c}$ : Switching frequency ( Hz )
(3) $\mathrm{V}_{\mathrm{BB}}$ power loss: $\mathrm{P}_{\mathrm{ibB}}$
$\mathrm{P}_{\mathrm{iBB}}=\mathrm{V}_{\mathrm{BB}} \times \mathrm{I}_{\mathrm{BB}}(\mathrm{W})$
$\mathrm{I}_{\mathrm{BB}}=\mathrm{V}_{\mathrm{BB}}$ supply current $(\mathrm{A}) *$ Supply current when all phases are off
(4) Steady-state power loss: Picc
$\mathrm{P}_{\mathrm{icc}}=\mathrm{V}_{\mathrm{cc}} \times \mathrm{I}_{\mathrm{cc}}(\mathrm{W})$
$\mathrm{I}_{\mathrm{cc}}=\mathrm{V}_{\mathrm{cc}}$ supply current (A) * Supply current during normal operation


Figure 4.4 Motor current waveform for power loss calculation

## 5. Application circuit example

### 5.1. Application circuit example



Figure 5.1 Application circuit example (for tripping the current limiter with an HVIPD)


Figure 5.2 Application circuit example (for tripping the current limiter with a motor controller IC or an MCU)

Table 5.1 shows typical external parts.

Table 5.1 External parts for the application circuit

| Part | Recommended Value | Purpose | Note |
| :--- | :--- | :--- | :--- |
| $\mathrm{C}_{1}, \mathrm{C}_{2}, \mathrm{C}_{3}$ | $25 \mathrm{~V} / 2.2 \mu \mathrm{~F}$ | Bootstrap capacitors | (Note 1) |
| $\mathrm{C}_{4}$ | $25 \mathrm{~V} / 10 \mu \mathrm{~F}$ | V $_{\text {CC }}$ voltage stability | (Note 2) |
| $\mathrm{C}_{5}$ | $25 \mathrm{~V} / 0.1 \mu \mathrm{~F}$ | V $_{\text {CC }}$ surge absorption | (Note 2) |
| $\mathrm{C}_{6}$ | $25 \mathrm{~V} / 1 \mu \mathrm{~F}$ | V REG voltage stability | (Note 2) |
| $\mathrm{C}_{7}$ | $25 \mathrm{~V} / 1000 \mathrm{pF}$ | V REG surge absorption | (Note 2) |
| $\mathrm{R}_{1}$ | $5.1 \mathrm{k} \Omega$ | DIAG pull-up resistor | (Note 3) |
| $\mathrm{R}_{2}$ | $10 \mathrm{k} \Omega$ | SD pull-up resistor | (Note 4) |
| $\mathrm{R}_{3}$ | $0.35 \Omega \pm 1 \%(1 \mathrm{~W})$ | Overcurrent detection | (Note 5) |

Note 1: The required bootstrap capacitor value varies, depending on the motor drive conditions. The capacitor is biased by $\mathrm{V}_{\mathrm{Cc}}$ and must be sufficiently derated.

Calculating the value of the bootstrap capacitor required
$C B=I B \times$ maximum high-side drive period $/\left(V_{C C}-V_{F}(B S D)+V_{F}(F R D)-13.5\right)(F)$
CB : Minimum capacitance of the bootstrap capacitor
IB: Maximum supply current of the high-side driver
$V_{F}(B S D)$ : Forward voltage of the bootstrap diode
$V_{F}$ (FRD): Forward voltage of the flywheel diode

Note 2: The capacitor values should be adjusted if noise occurs under actual usage conditions. Place the capacitors as close as possible to the IC leads to minimize ripple noise.

Note 3: The DIAG pin has an open-drain configuration. When unused, the DIAG pin should be connected to GND. The maximum rated current of the DIAG pin is 20 mA . Therefore, when it is pulled up to 7 V , the minimum resistor value is $350 \Omega$.

Note 3 and Note 4: The recommended pull-up resistor values are:
$\mathrm{R}_{1}: 1 \mathrm{k} \Omega$ to $10 \mathrm{k} \Omega$
$\mathrm{R}_{2}: 5 \mathrm{k} \Omega$ to $15 \mathrm{k} \Omega$

Note 5: The current-sensing level is expressed as: $\mathrm{I}_{\mathrm{O}}=\mathrm{V}_{\mathrm{R}} \div \mathrm{R}_{3}$ ( $\mathrm{V}_{\mathrm{R}}=0.5 \mathrm{~V}$ typical)
In order that IS1/IS2/IS3 terminals which connects shunt resistance may avoid malfunction and destruction, please wiring length be short and design.
When wiring length becomes long, please attach the diode for surge protection between IS1/IS2/IS3 terminals -GND terminal.

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